

The application of seismic derived rock properties in predicting Duvernay Induced Fractures

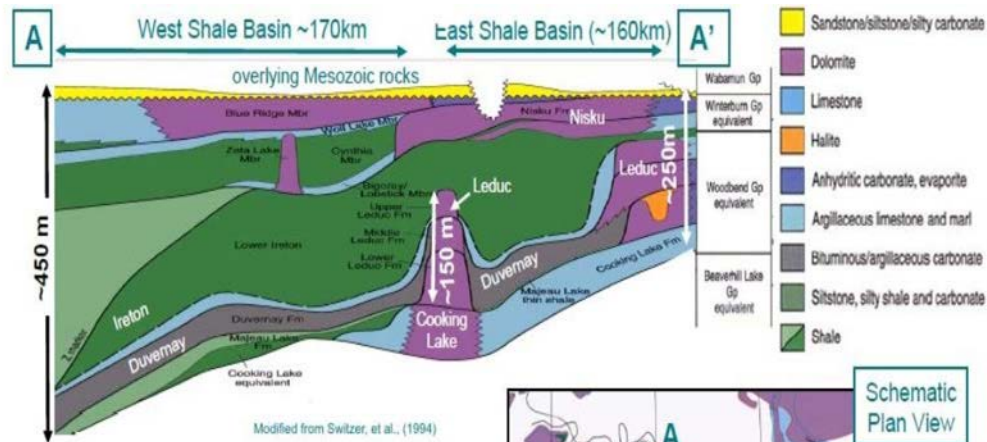
Ronald Weir, D. Eaton, L. Lines, D. Lawton

Introduction

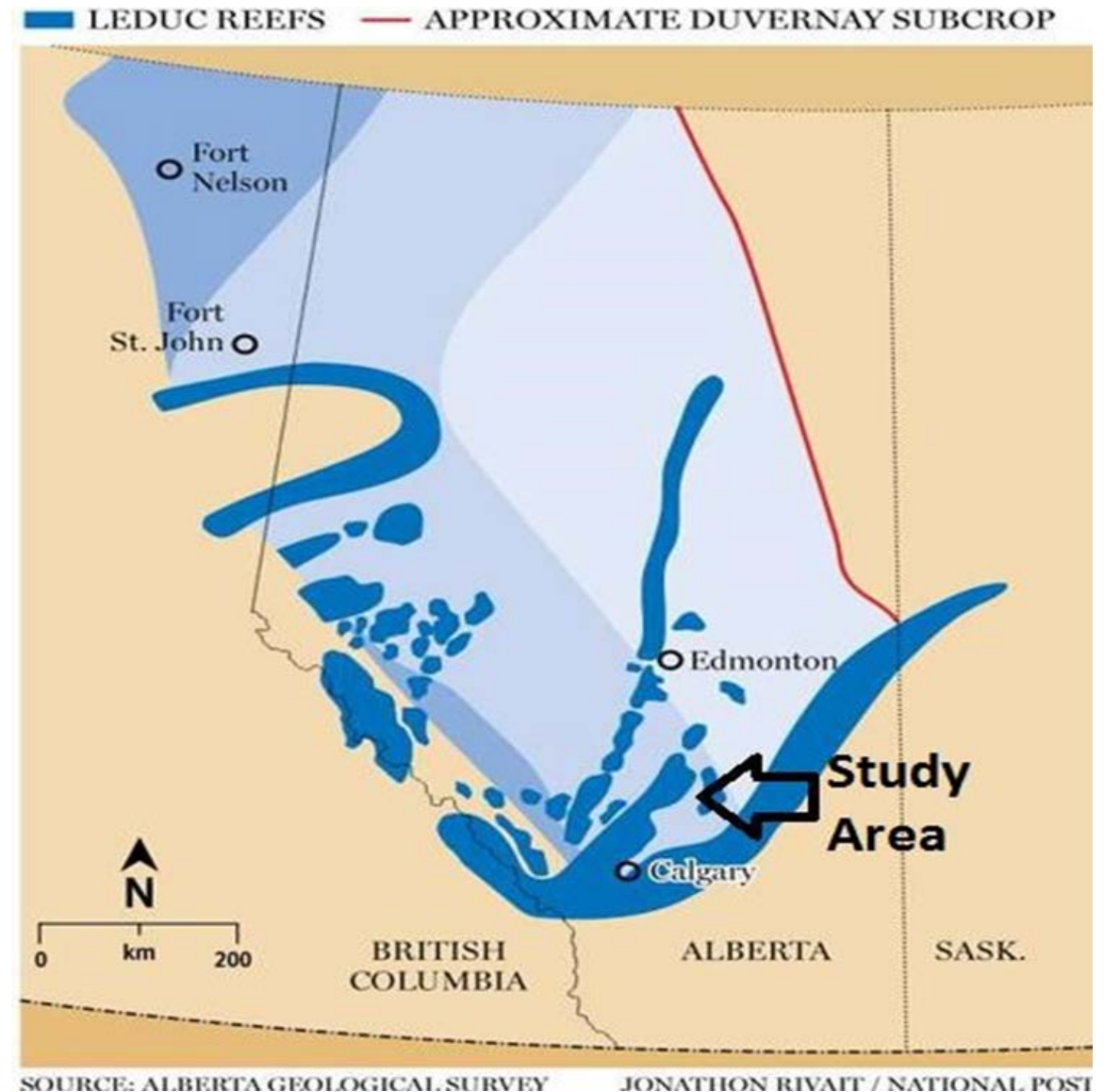
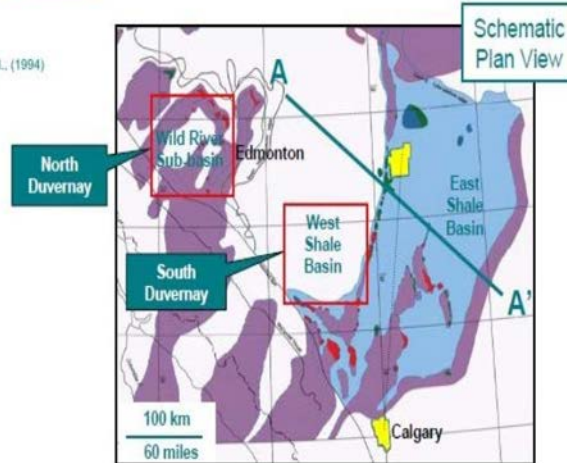
- Overview of Duvernay Geology
 - Regional Framework
 - Modern Analogue
 - Core work
 - Theoretical Rock properties
- Current development practices
 - Horizontal drilling, microseismic results
- Seismic inversion analysis
 - Simultaneous inversion
 - Derivation of rock properties
- Uses and applications
 - Implications of reservoir characteristics
 - Future work

Duvernay Formation mature oil window

Duvernay Formation Depositional Environment



- Both North Duvernay (Wild River) and South Duvernay (West Shale Basin) were centered in areas adjacent to reef development
- Reefs created restricted basin conditions, where organic productivity was high resulting in thick, high TOC shale deposits



Great Barrier Reef, modern analogue to the Leduc / Duvernay



Duvernay /Leduc modern analogue



Kaybob area, core analysis of rock properties.

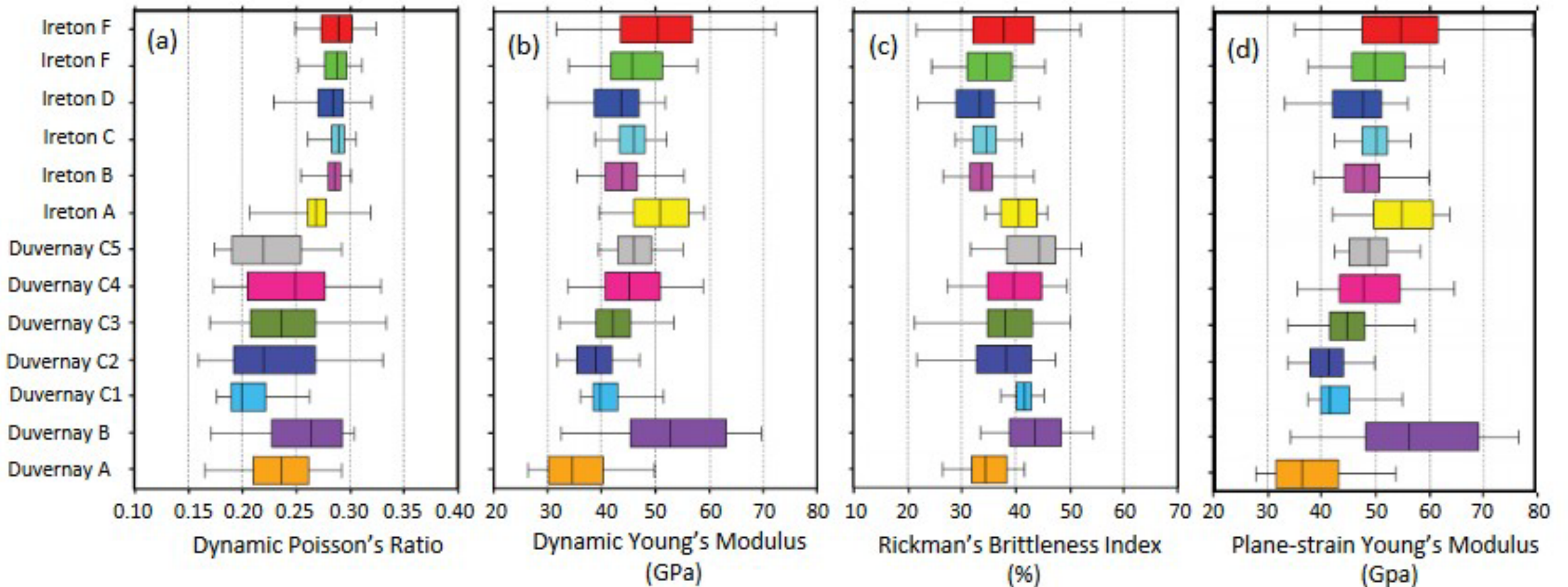
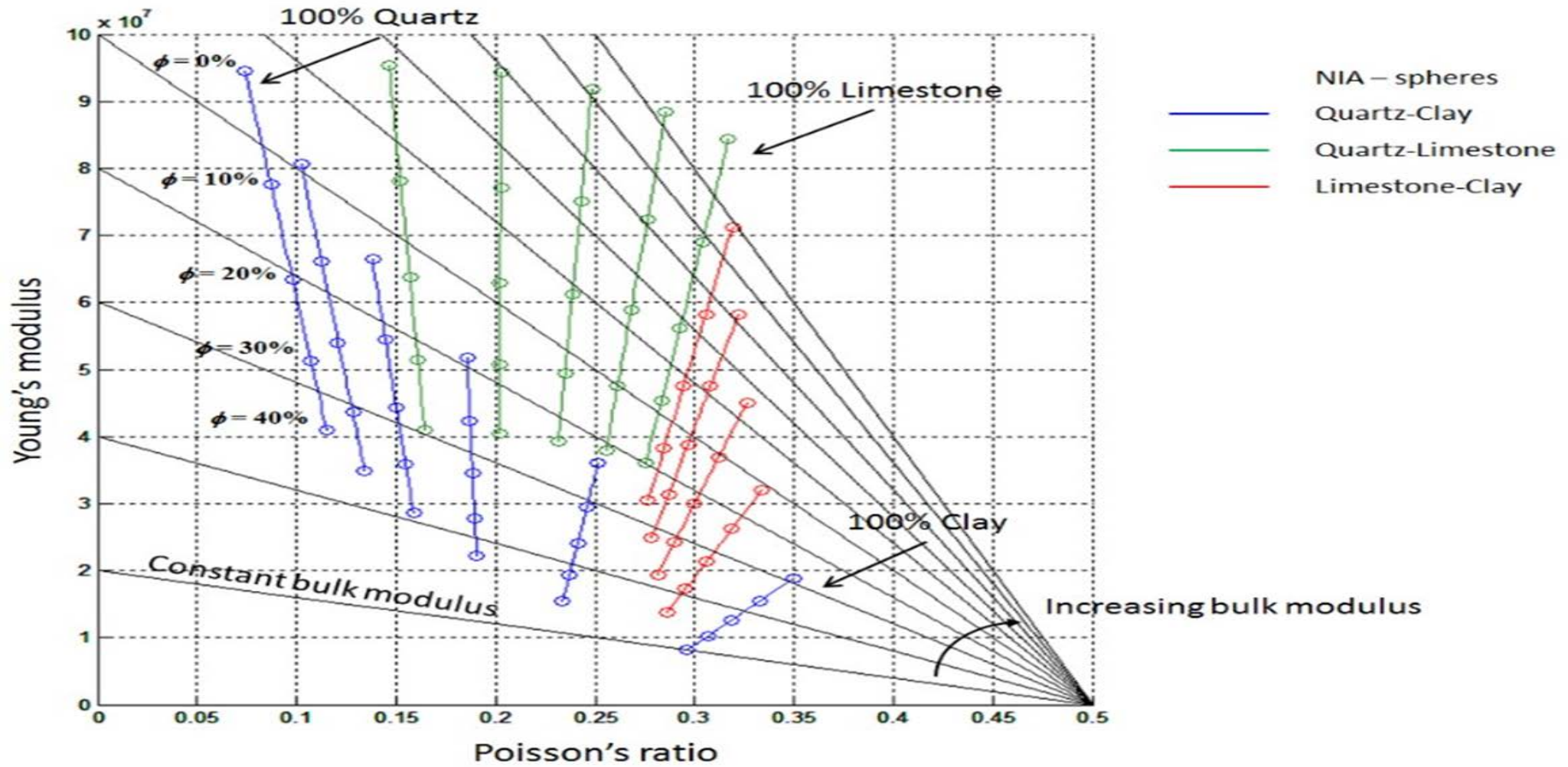


Figure 1. Mechanical properties calculated based on sonic logs for 26 wells for the Duvernay and Ireton formations: (a) dynamic Poisson's ratio, (b) dynamic Young's Modulus, (c) Rickman's brittleness Index, and (d) plane-strain Young's modulus.

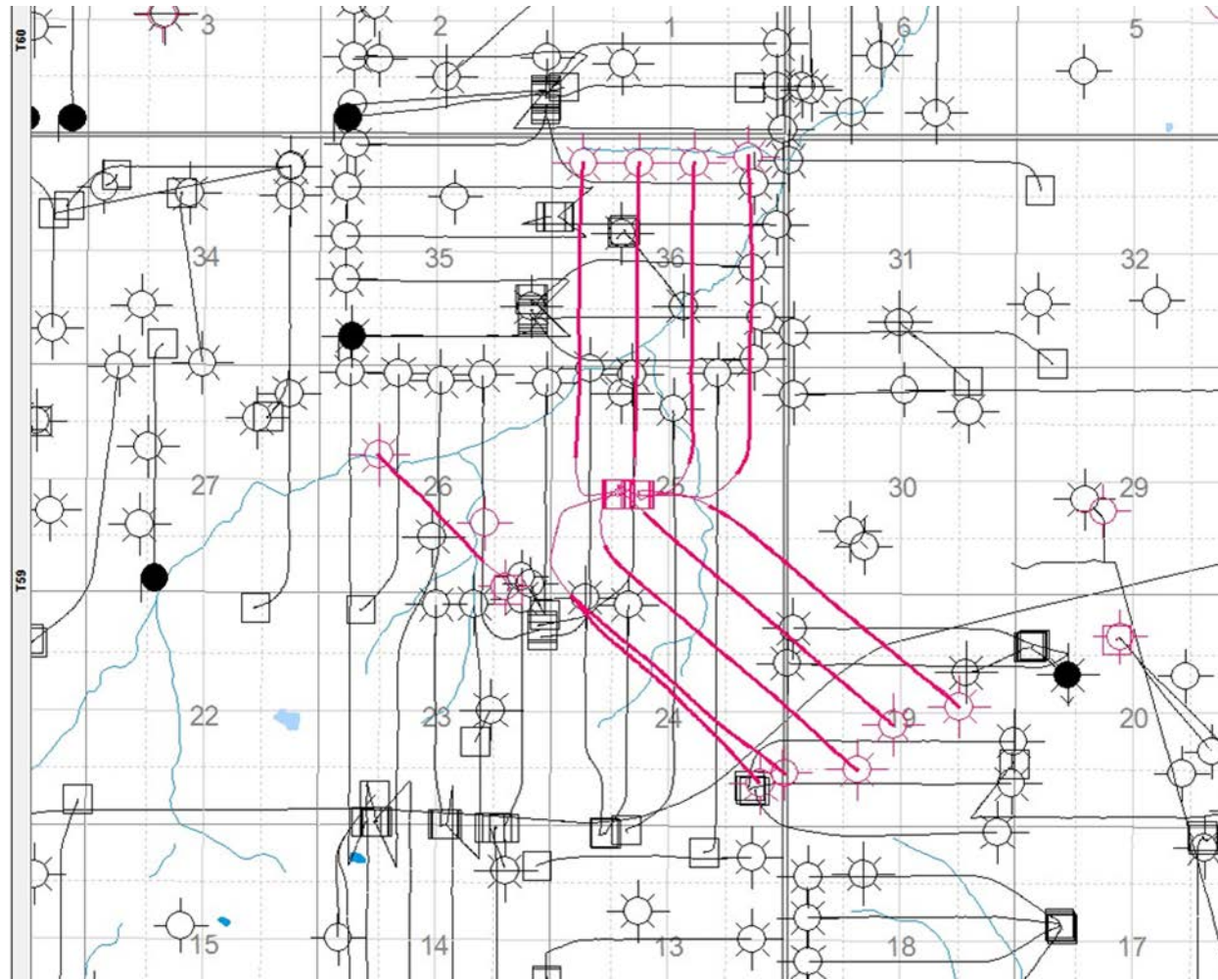
Amy D. Fox, Mehrdad Soltanzadeh Canadian Discovery Ltd.

Theoretical calculation of rock properties

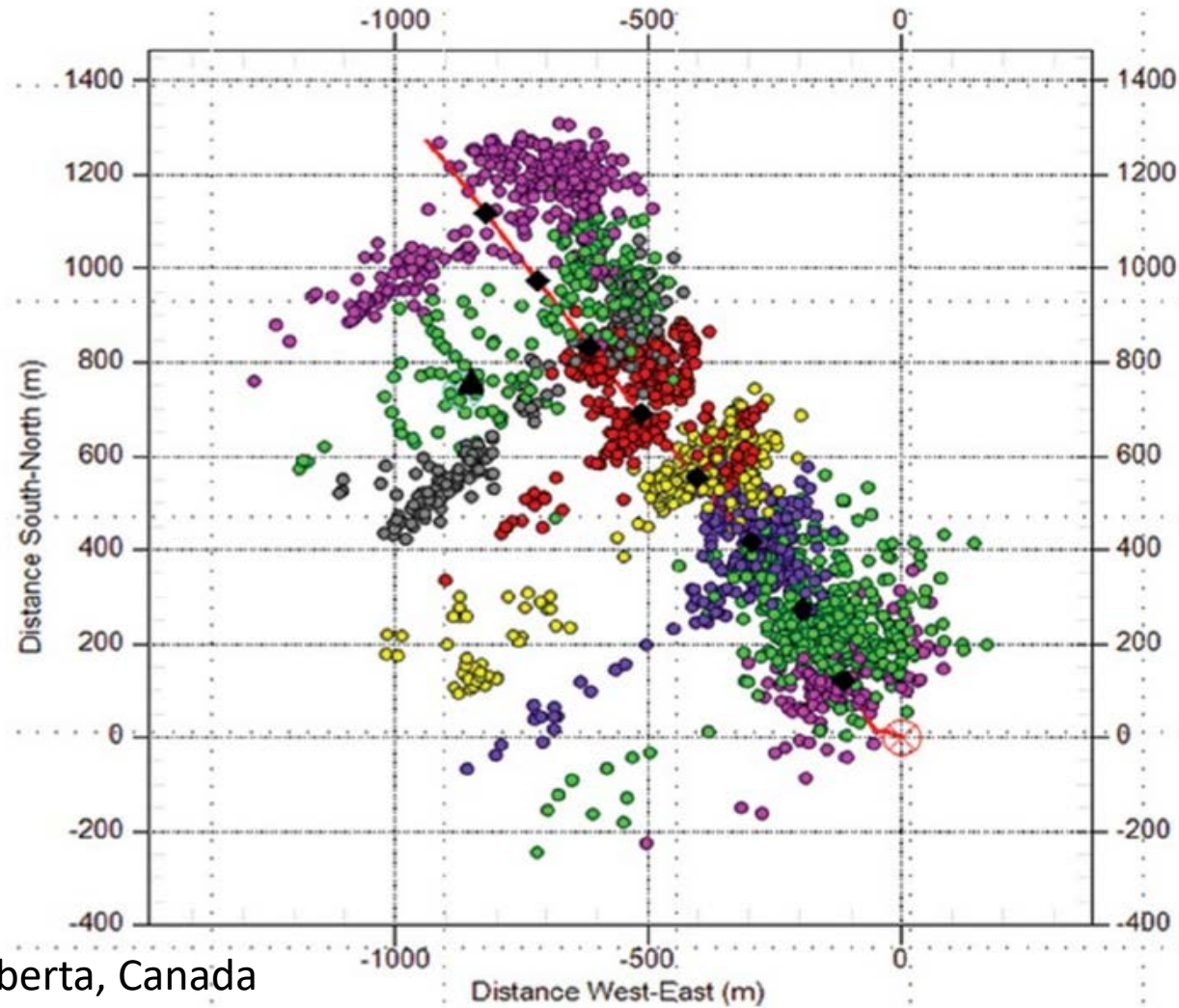


Cho Et al, GeoConvention 2014 FOCUS

Duvernay Horizontal plan, Kaybob/Bigstone

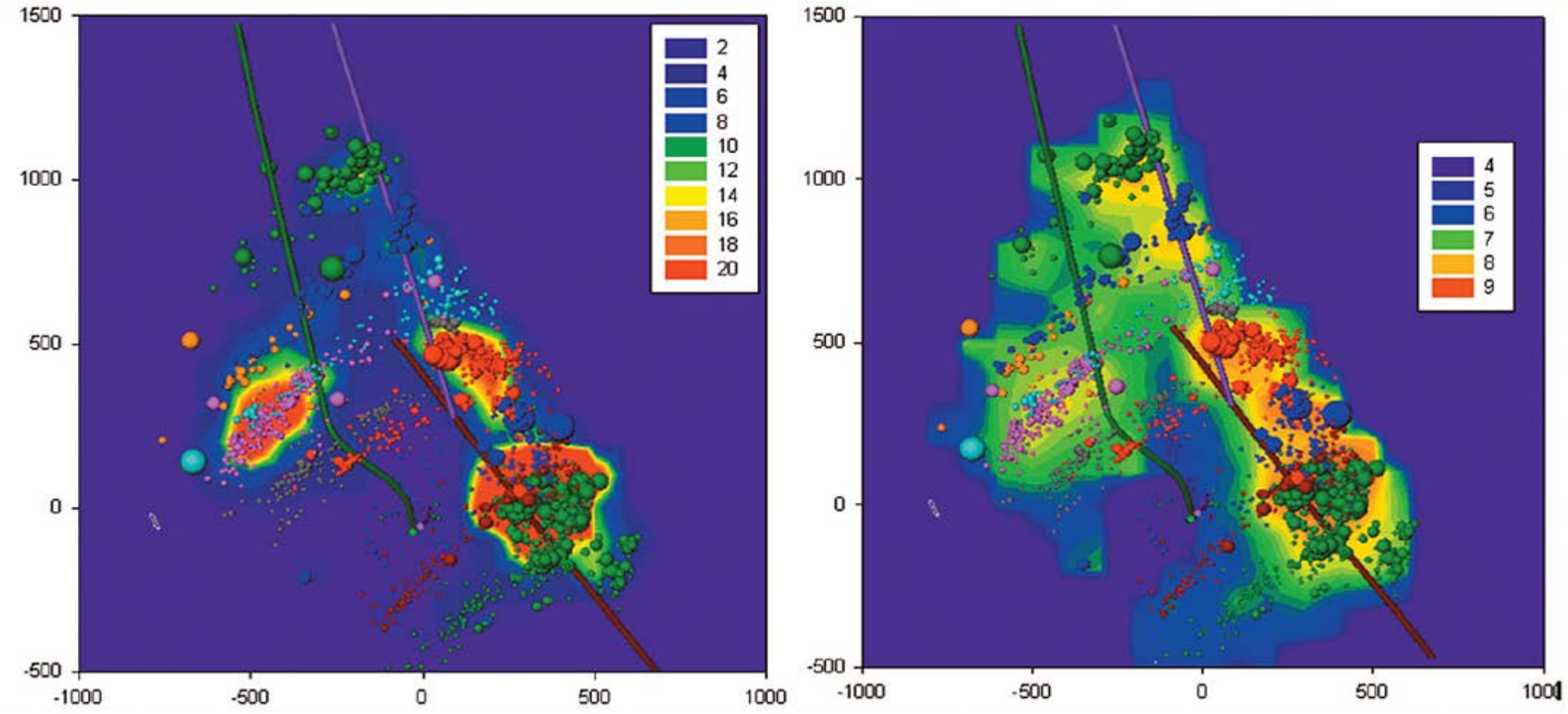


Alberta Example, Montney shale , Microseismic recorded



Shawn C. Maxwell
Schlumberger, Calgary, Alberta, Canada
[Nov 2011 | VOL. 36 No. 09](#)

Variations in microseismic activity in the Montney Shale

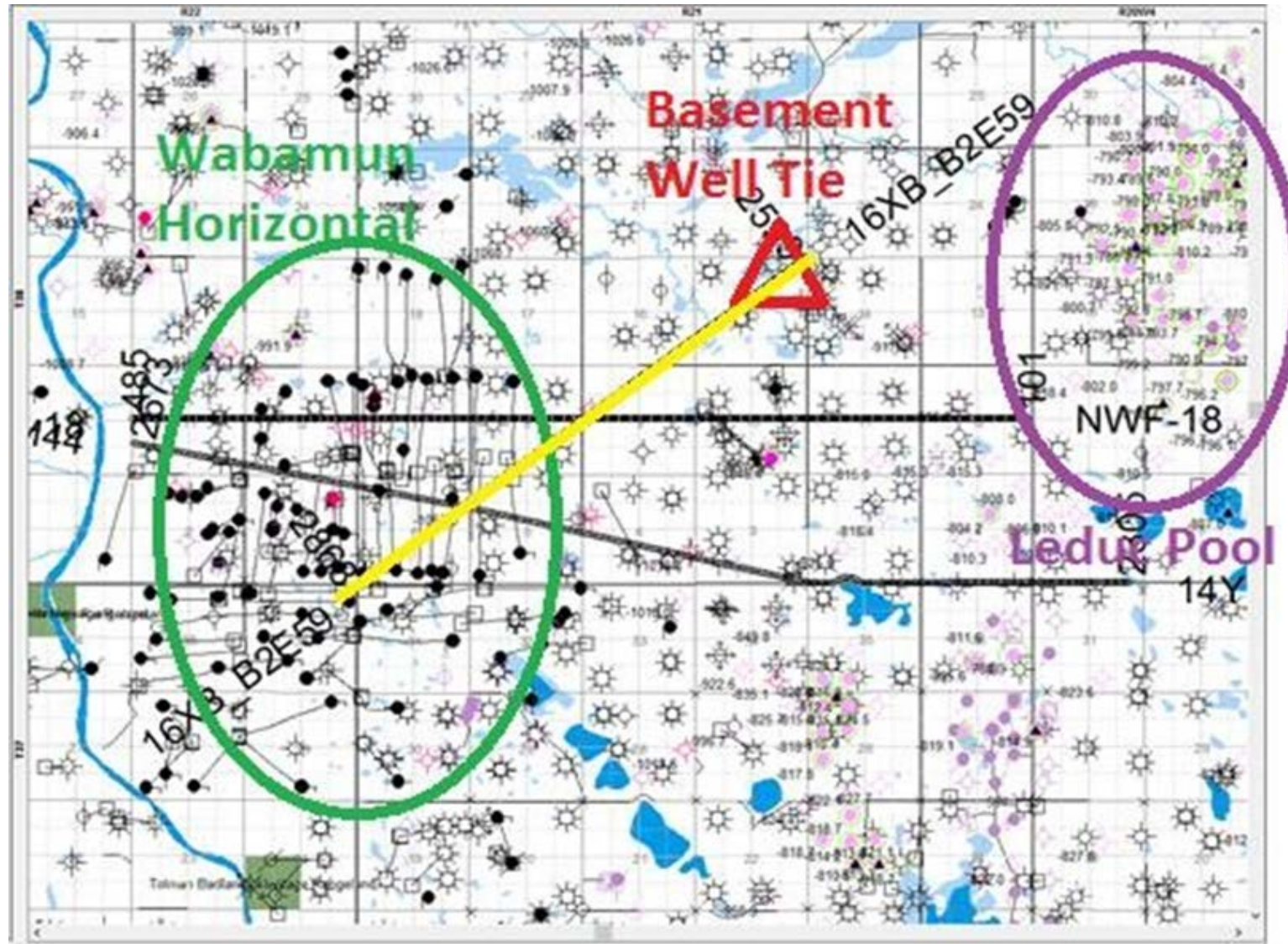


Shawn C. Maxwell

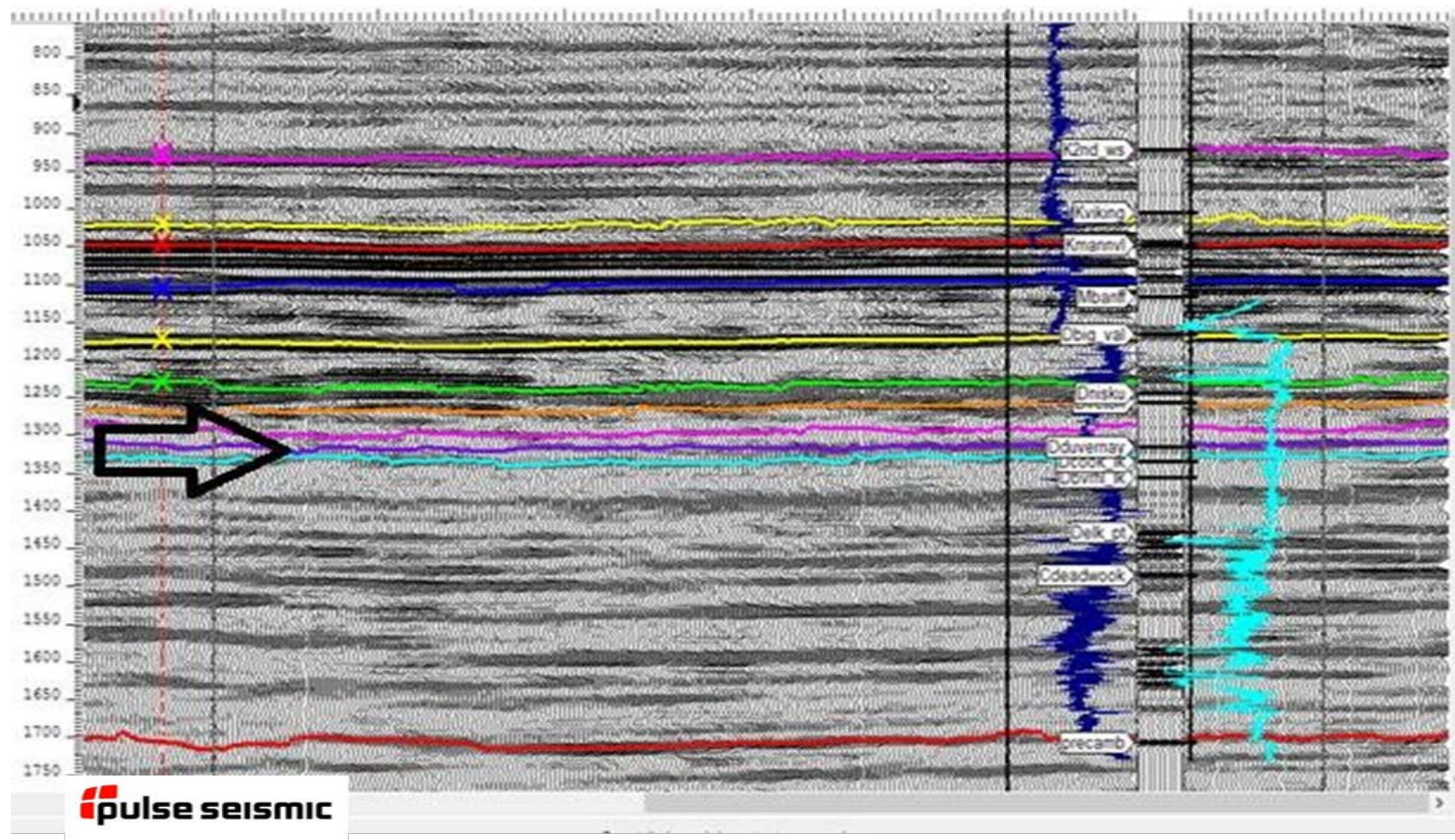
Schlumberger, Calgary, Alberta, Canada

Oct 2011 | VOL. 36 No. 08 |

Study area, East – Central Alberta



Large scale synthetic tie, highlighting the zone of interest



Prestack modeling and inversion

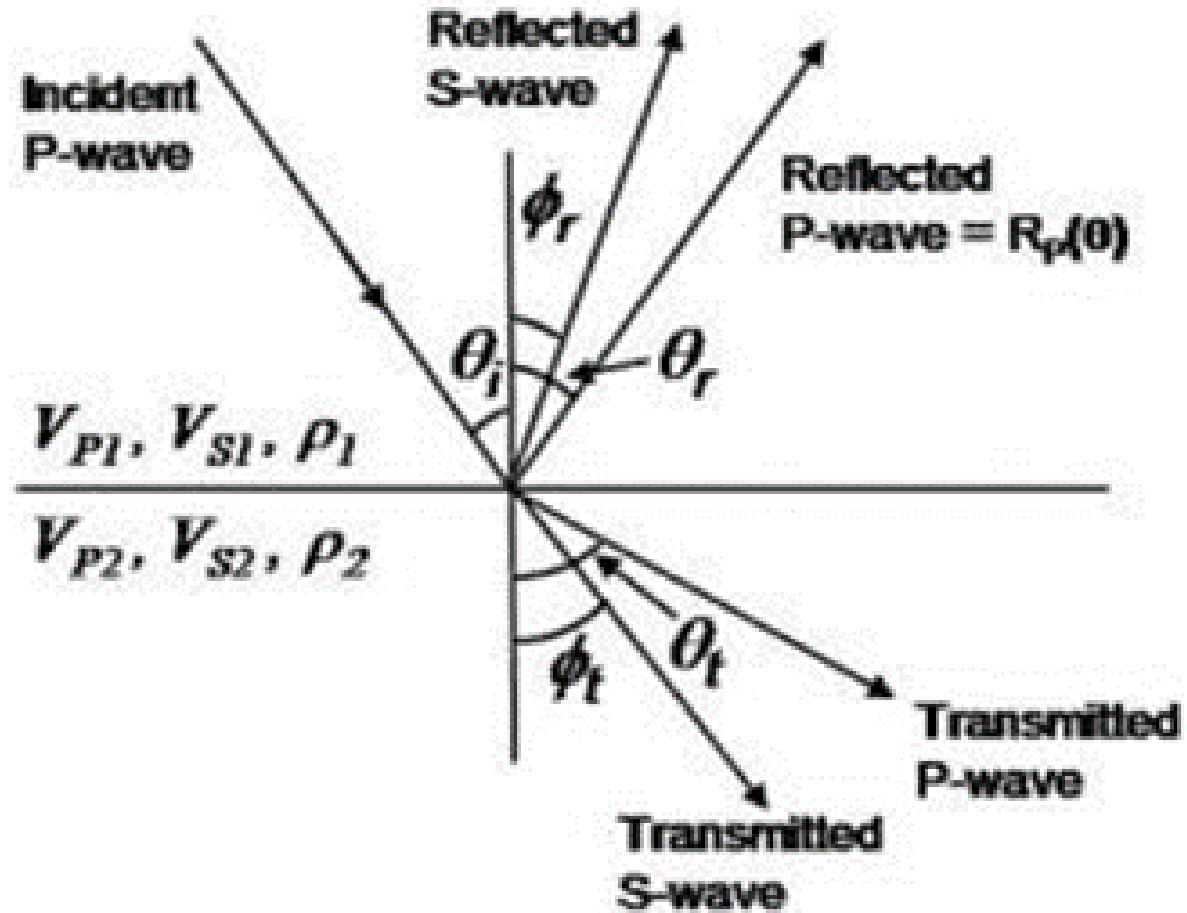
We start with Fatti's version of the Aki-Richards' equation. This models reflection amplitude as a function of incident angle:

$$R_{PP}(\theta) = c_1 R_P + c_2 R_S + c_3 R_D$$

where:

$$\begin{aligned} c_1 &= 1 + \tan^2 \theta \\ c_2 &= -8\gamma^2 \sin^2 \theta \\ c_3 &= -\frac{1}{2} \tan^2 \theta + 2\gamma^2 \sin^2 \theta \\ \gamma &= \frac{V_S}{V_P} \end{aligned}$$

$$\begin{aligned} R_P &= \frac{1}{2} \left[\frac{\Delta V_P}{V_P} + \frac{\Delta \rho}{\rho} \right] \\ R_S &= \frac{1}{2} \left[\frac{\Delta V_S}{V_S} + \frac{\Delta \rho}{\rho} \right] \\ R_D &= \frac{\Delta \rho}{\rho} \end{aligned}$$



Reflection PP calculation

From the Fatti's version of the Aki-Richards' equation:

$$R_{PP}(\theta) = c_1 R_P + c_2 R_S + c_3 R_D$$

Where,

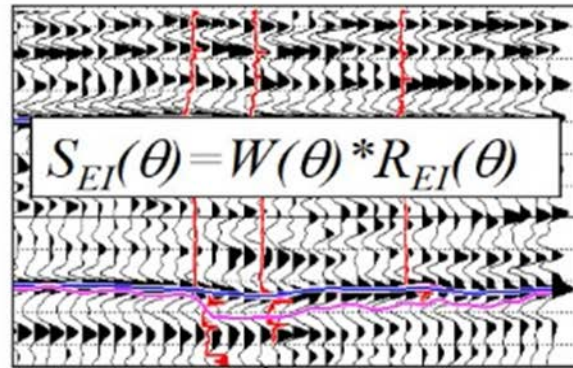
$$c_1 = 1 + \tan^2 \theta, \quad c_2 = -8\gamma^2 \sin^2 \theta, \quad c_3 = -\frac{1}{2} \tan^2 \theta + 2\gamma^2 \sin^2 \theta$$

$$R_P = \frac{1}{2} \left[\frac{\Delta\rho}{\rho} + \frac{\Delta V_P}{V_P} \right], \quad R_S = \frac{1}{2} \left[\frac{\Delta\rho}{\rho} + \frac{\Delta V_S}{V_S} \right], \quad R_D = \frac{\Delta\rho}{\rho}$$

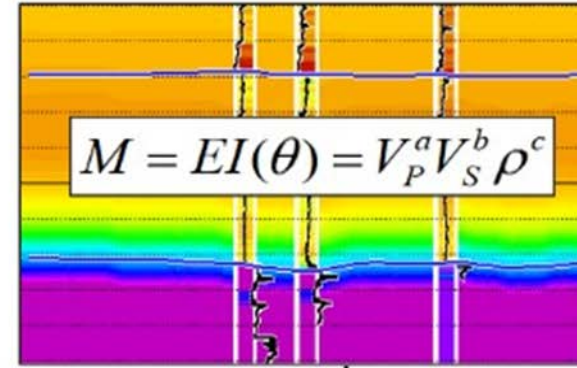
These equations form the basis to estimate the PP and PS reflect derived from sonic, shear and density logs.

P, S, and density inversion workflow

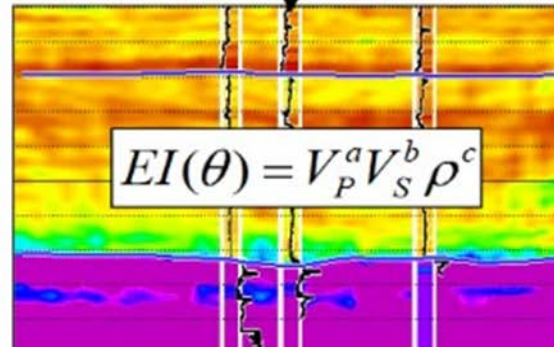
(1) Optimally process the seismic data



(2) Build model from picks and impedances

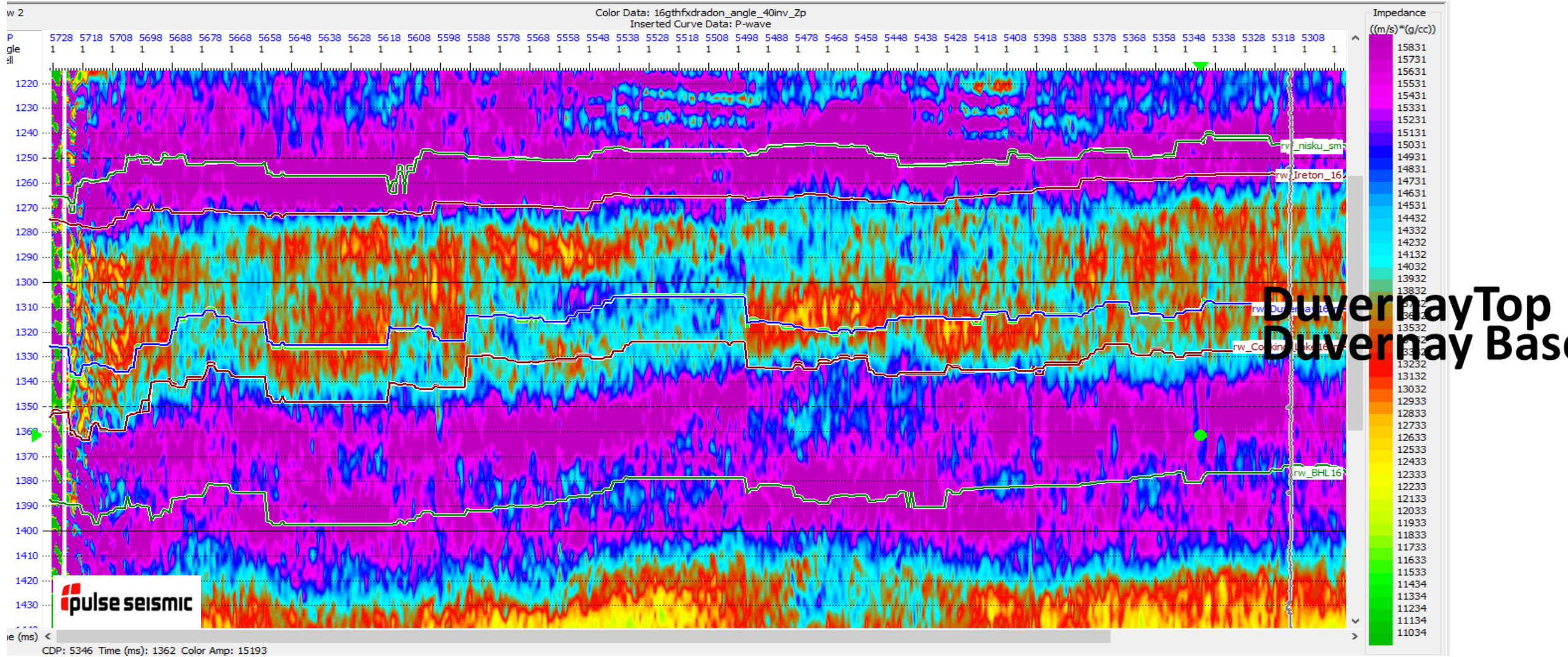


(3) Iteratively update model until output synthetic matches original seismic data.



In elastic impedance inversion the seismic, model and output are as shown here.

Prestack Inversion, PP reflectivity



Youngs Modulus and Poisson Ratio Calculation from inversion

Related equations are defined as follows:

$$\text{Poisson's Ratio: } PR = \frac{0.5 * \left(\frac{Vp}{Vs}\right)^2 - 1}{\left(\frac{Vp}{Vs}\right)^2 - 1}; \text{ Closure Stress Ratio: } CSR = \frac{PR}{1 - PR}$$

$$\text{Young's Modulus: } E = \frac{2 * Z_s^2 * (1 + PR)}{\text{Density}}; \rho E = 2 * Z_s^2 * (1 + PR)$$

$$\text{Brittleness : } BRI = 100 * \left(w * \frac{(PR_{max} - PR)}{PR_{max} - PR_{min}} + (1 - w) * \frac{(E - E_{min})}{E_{max} - E_{min}} \right)$$

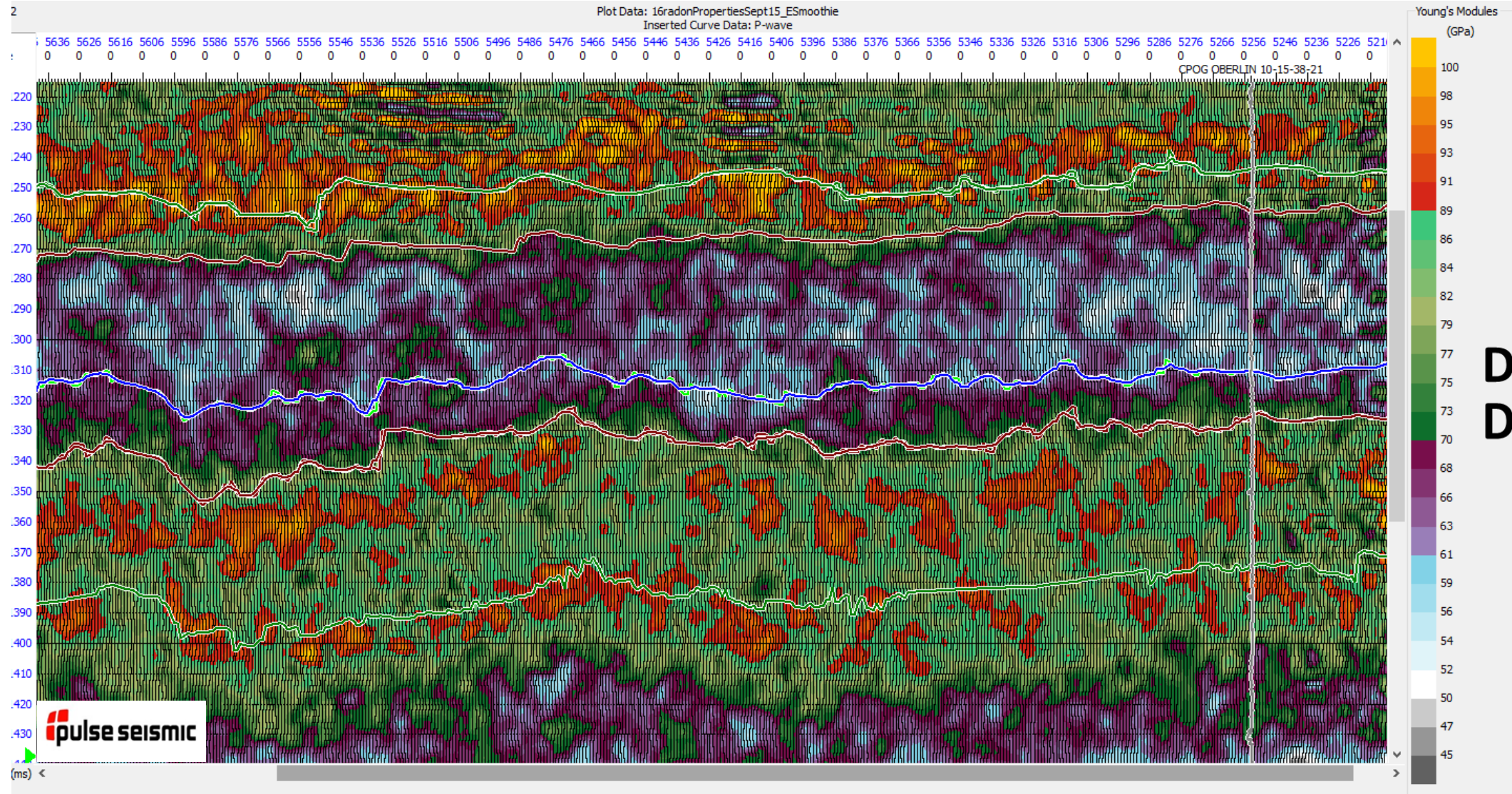
$$\text{Brinell Hardness Number : } BHN = 75.156 * E + 18.21$$

The default impedance unit used in the equation is (m/s)*(kg/m³);

Default velocity unit is (m/s); Default density unit is (kg/m³).

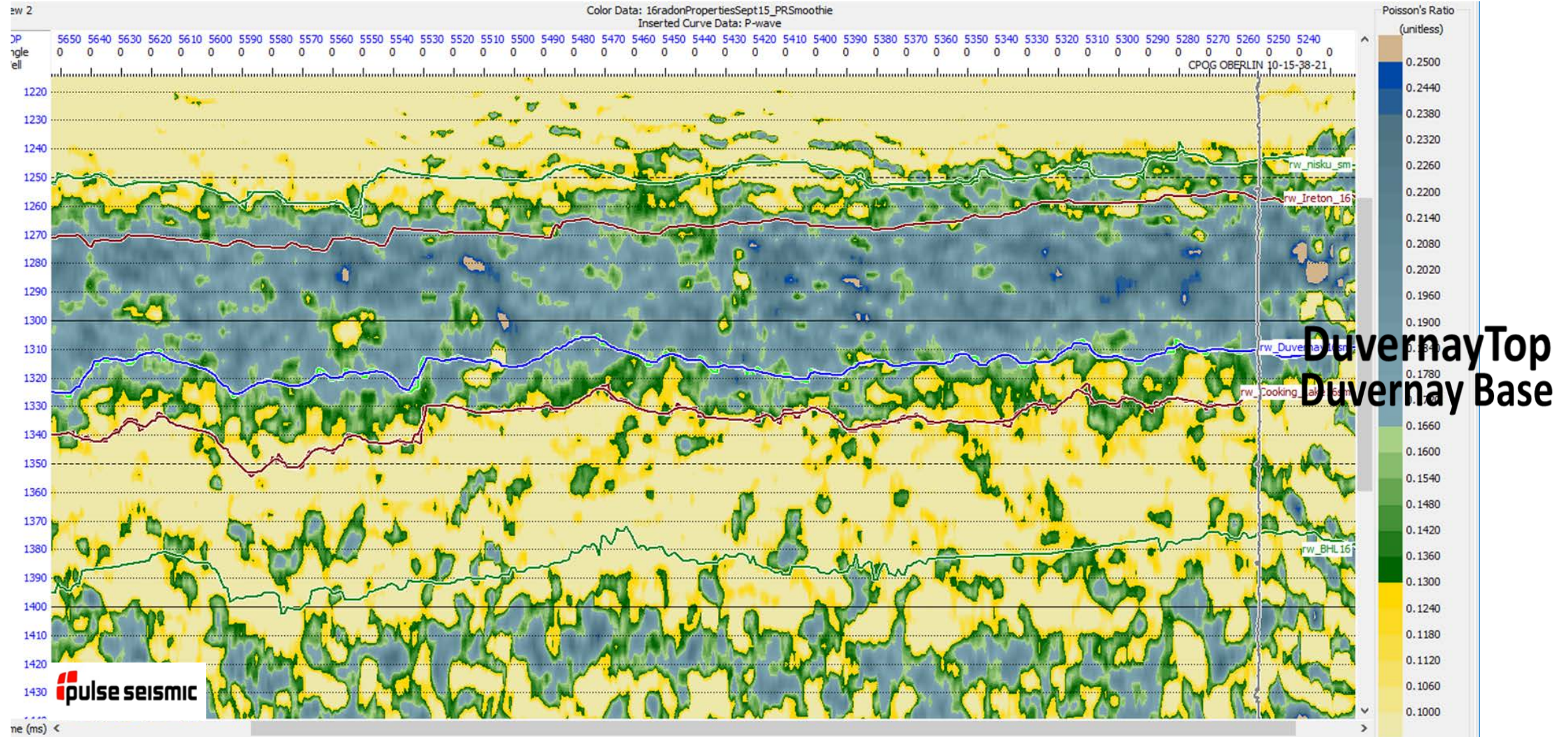
Input values in other units will be converted automatically.

Young's Modulus derived from inversion



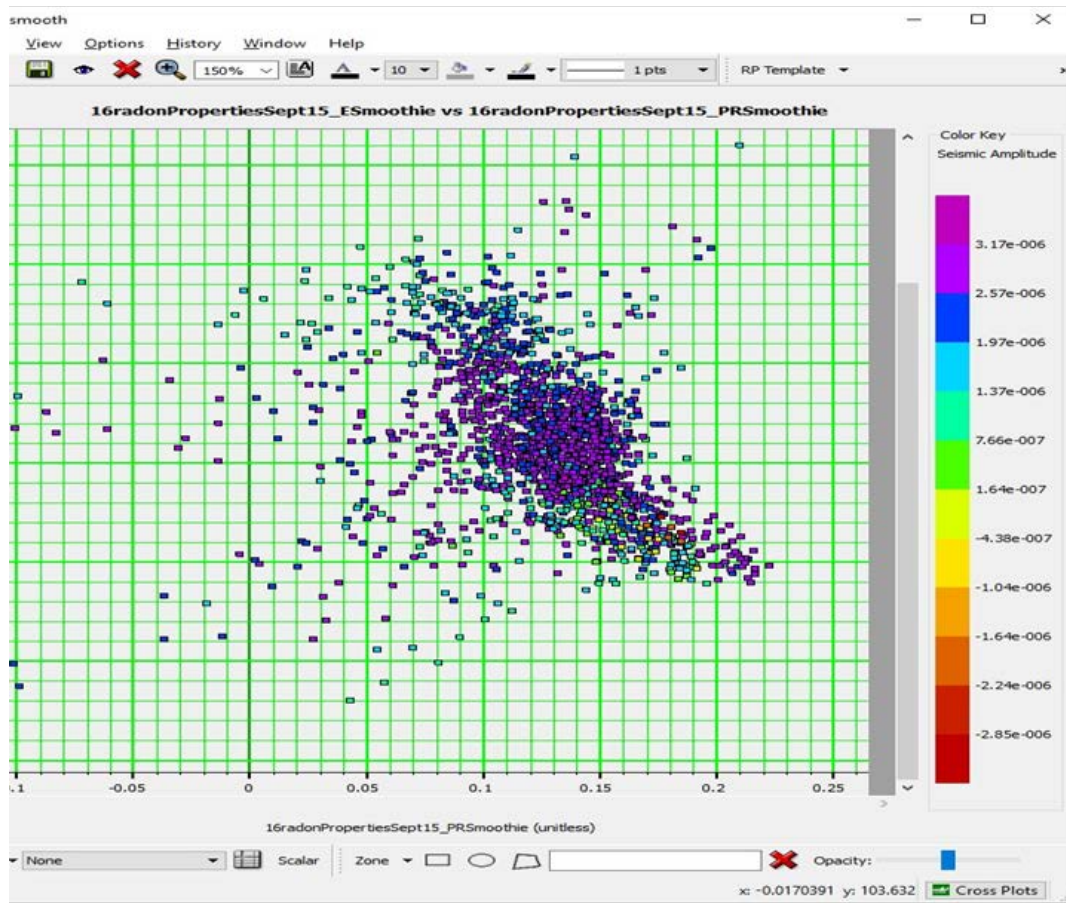
DuvernayTop
Duvernay Bas

Poisson's Ratio derived from prestack inversion



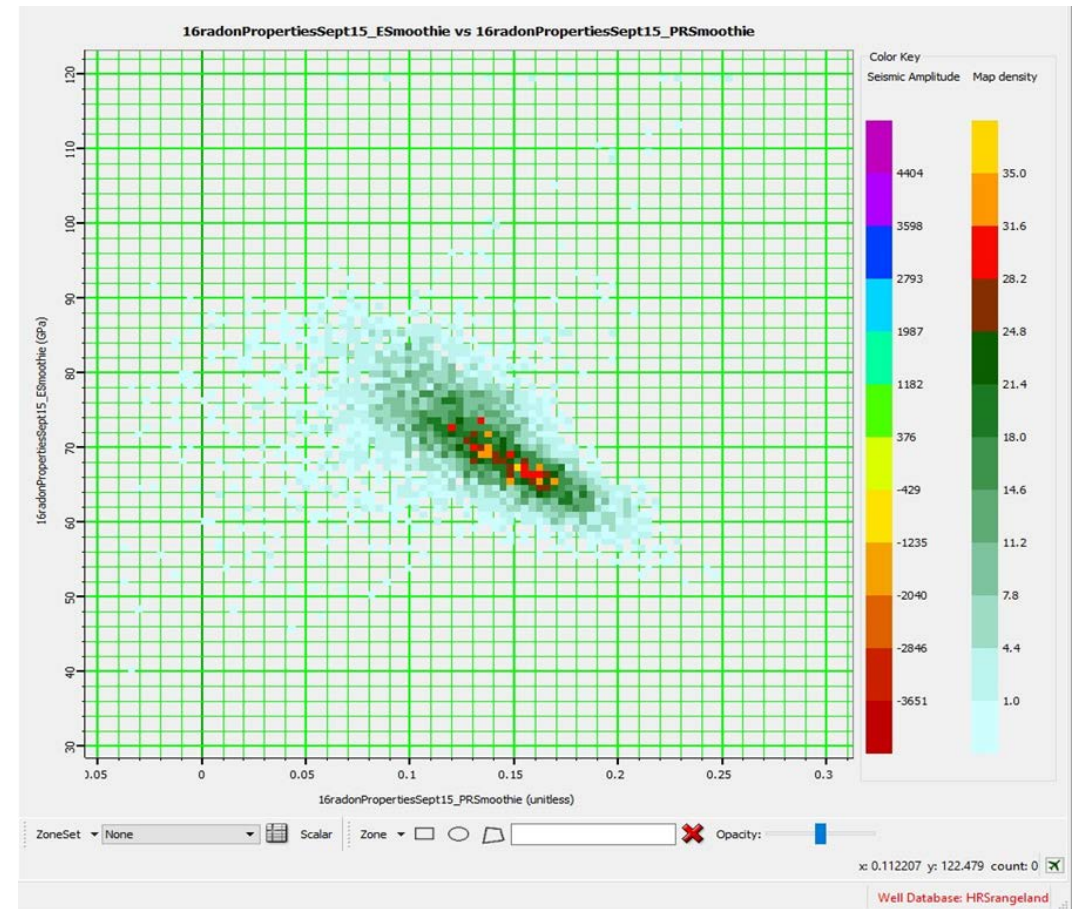
Cross Plot of Poisson Ratio Vs Young's Modulus, Duvernay interval

Young's Modulus



Poisson's Ratio

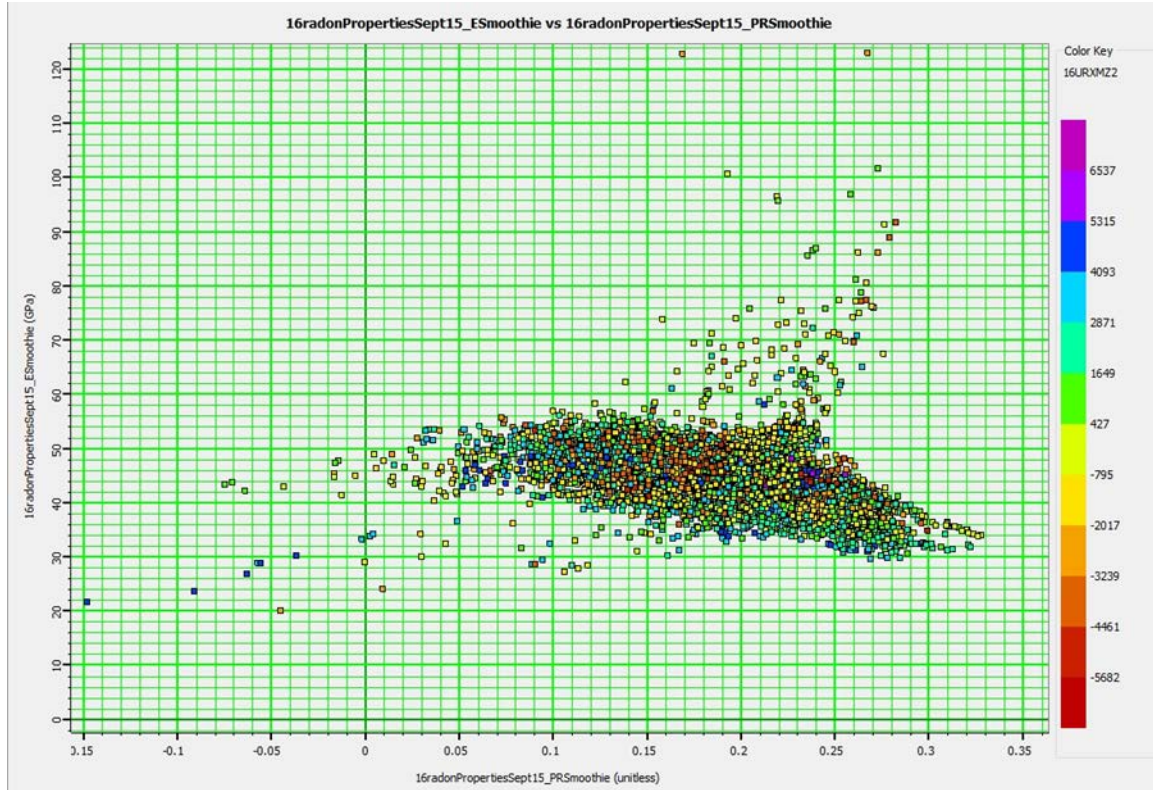
Young's Modulus



Poisson's Ratio

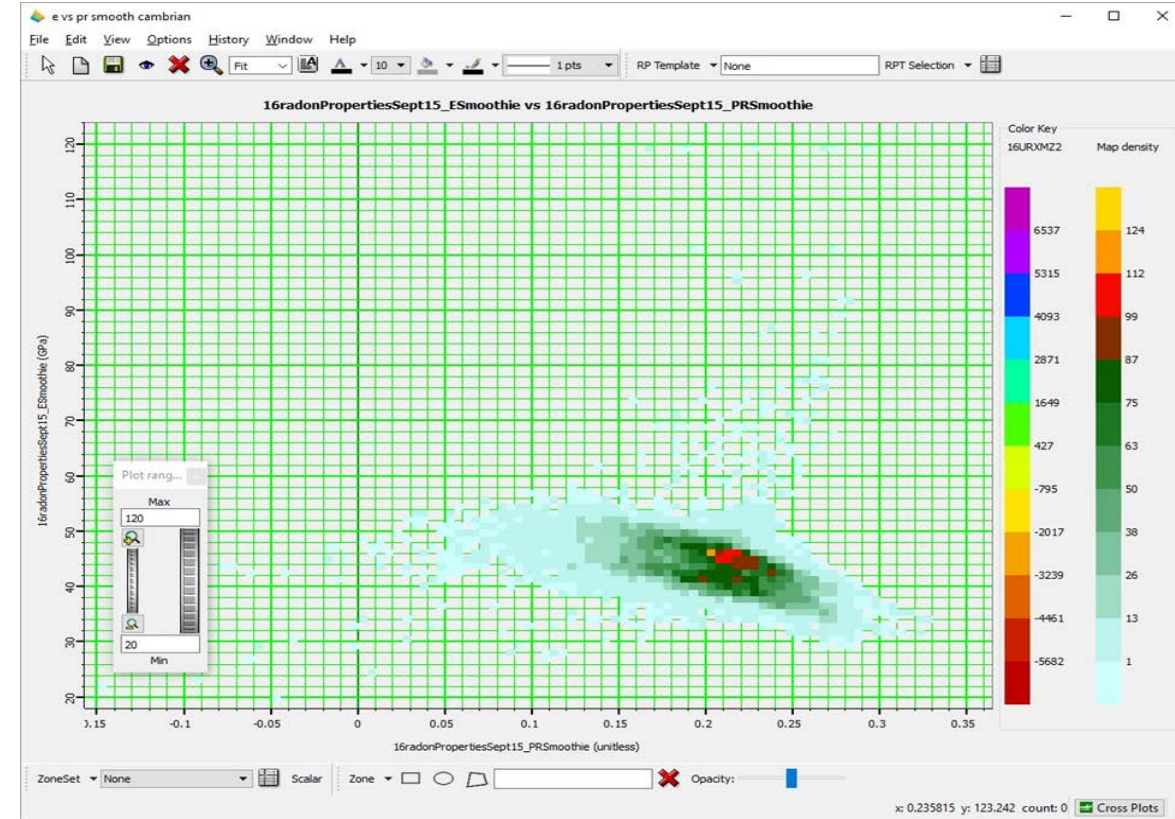
Cross Plot, Poisson Ratio Vs. Young's Modulus, Cambrian

Young's Modulus



Poisson's Ratio

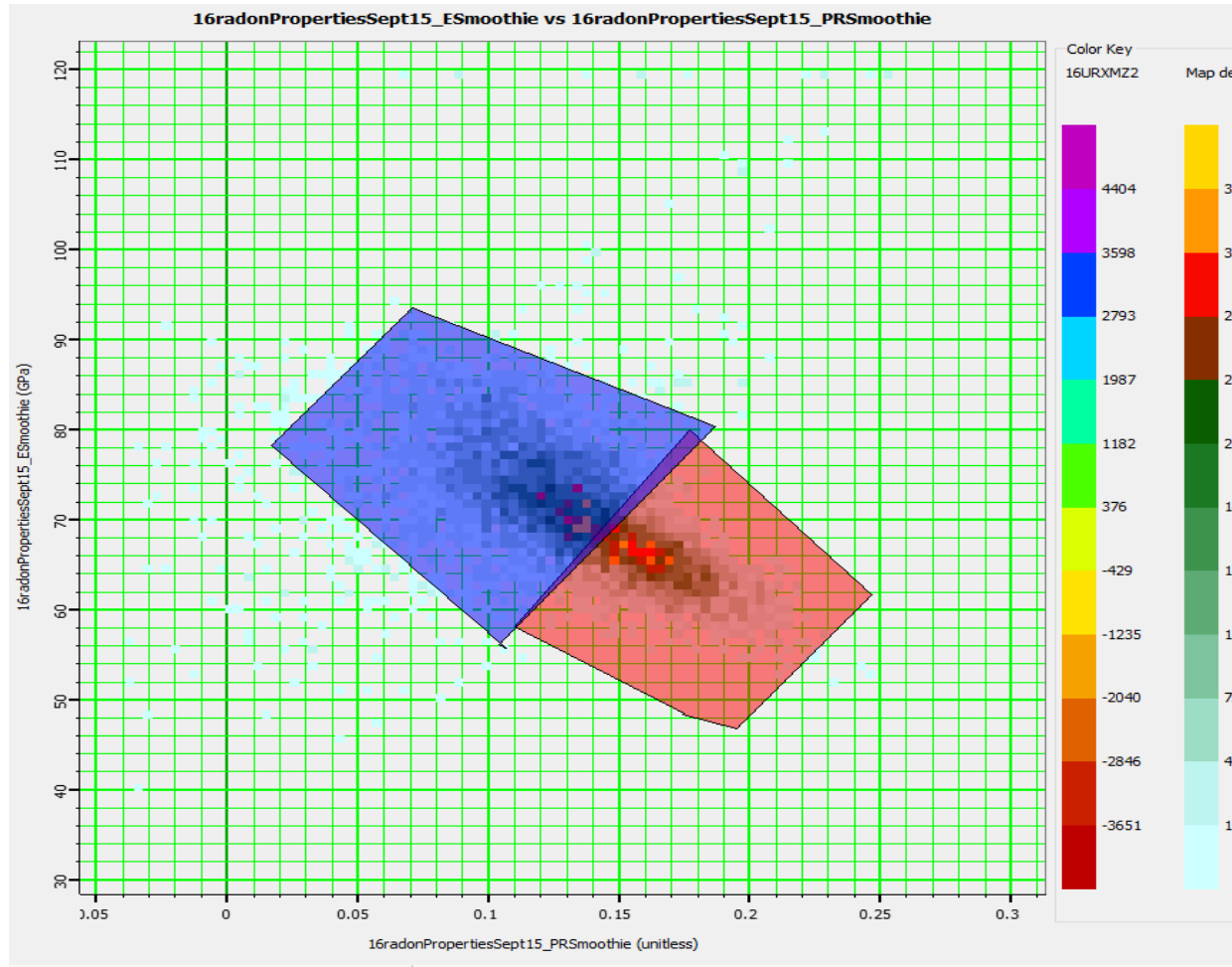
Young's Modulus



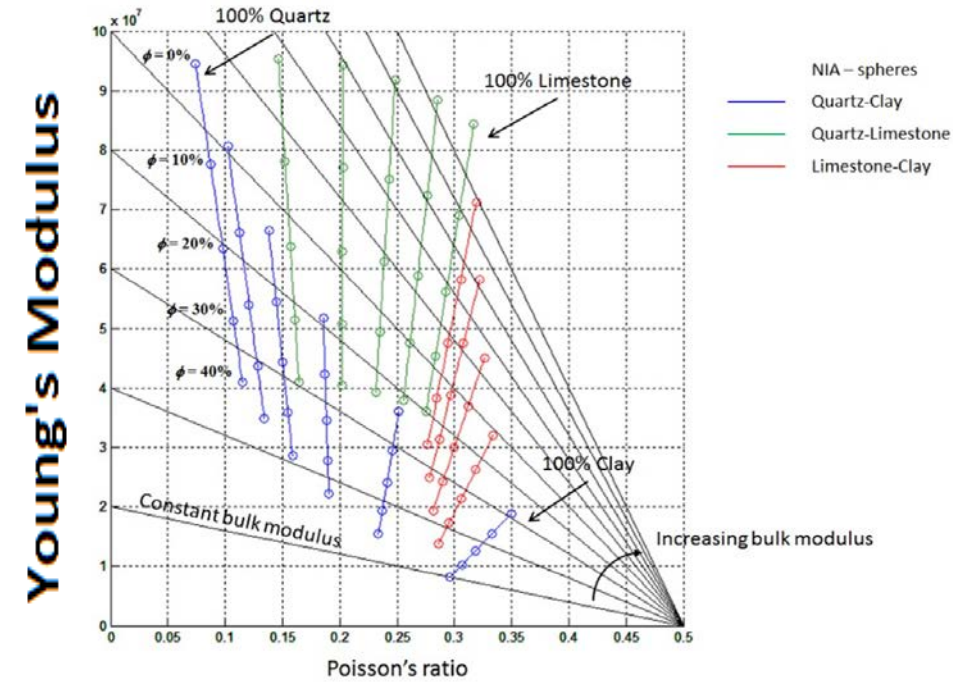
Poisson's Ratio

Derived and theoretical rock properties, Duvernay Formation

Young's Modulus

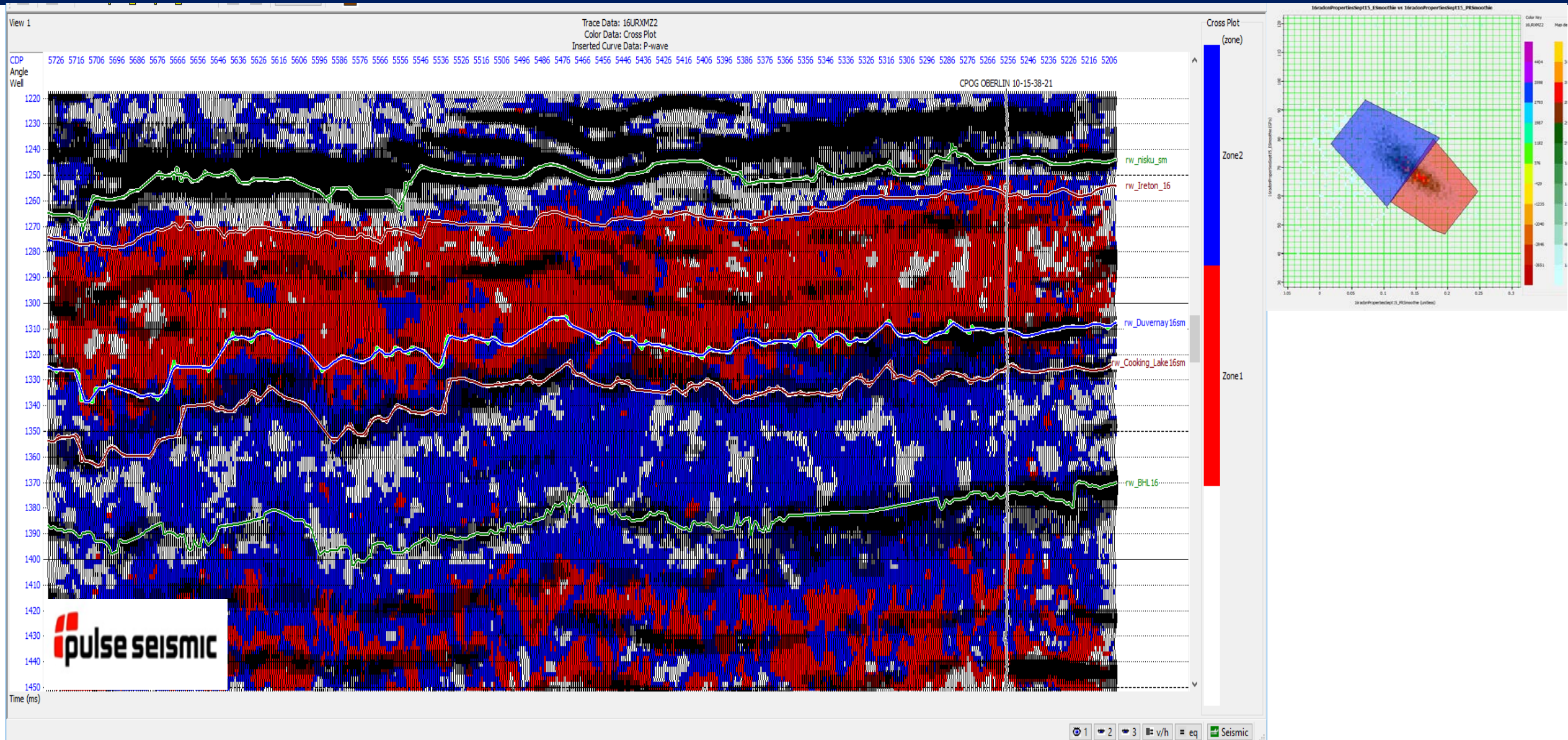


Poisson's Ratio

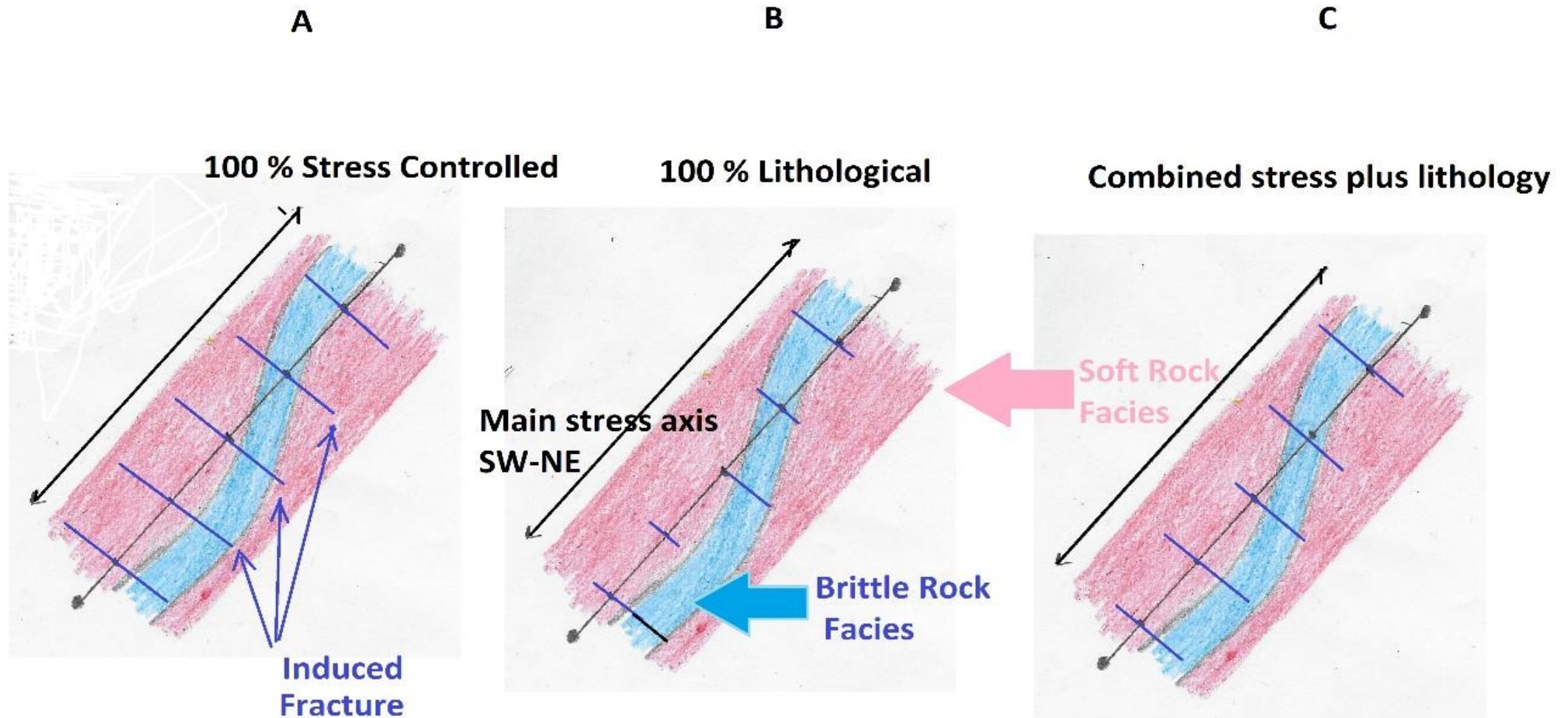


Poisson's Ratio

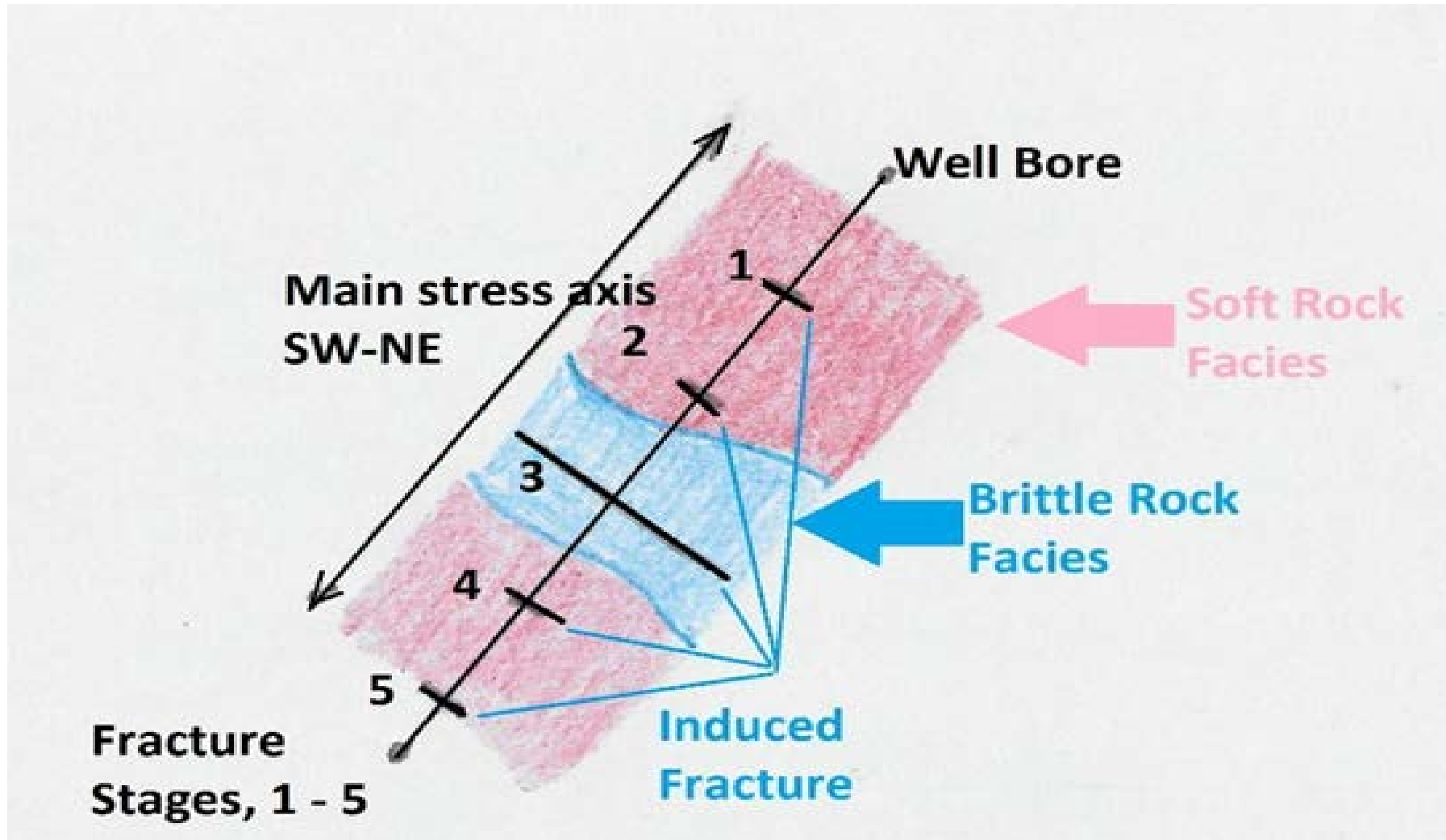
Blue areas are high brittleness, Red areas are low brittleness



Estimated response to fracture stimulation based on brittleness



Geologically defined prediction for induced fractures



Conclusions

- Reservoir attributes can readily be extracted from prestack data
- Wells can be better positioned based on rock parameters
- Reservoir characterization may be able to explain the variable fracture patterns and productivity of horizontal wells

Future work

- A 3-D data set has become available in Bigstone, with well control and ongoing microseismic monitoring
- This data set will be analyzed using the same methodology outlined in this presentation, with the incorporation of microseismic data.
- I expect to have results late 2017, or early 2018.

- **TECHNICAL SOFTWARE USED**
- Geoview (HRS), pre and poststack inversion
- Geoscout, Well grid and culture data base, LAS files, production and perforation information
- Seisware, Conventional seismic interpretation
- Vista, prestack data preparation.

Acknowledgements

- Dr. Brian Russell, technical advice and consultations
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- Statcom, access to their reprocessing facilities, Peter Snethledge, Tor Hagland
- Pulse Seismic Inc., Proprietary data provided as a contribution to the University of Calgary/CREWES

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