

Plane-wave reflection coefficients for anisotropic media *et al.*

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WARNING

This presentation contains
slides of mathematical
expressions which may be
offensive to some.

Viewer discretion is advised.

Outline

- Programming plane-wave reflection coefficients for anisotropic media
- Zoeppritz Explorer updates
- Fluid Properties calculator
- Hodogram Explorer
- Papers:
 - Ursenbach & Haase: “Plane-wave reflection coefficients for anisotropic media: Practical implementation”
 - Ursenbach & Lawton: “Seismic modeling of acid-gas injection in a deep saline reservoir”
 - Ursenbach: “New and updated web applet Explorers”

From DATA to PLAY

- DATA
- DATE
- DARE
- DIRE
- DIRT
- DIET
- DUET
- SUET
- SUED
- SLED
- PLED
- PLOD
- PLOY
- PLAY

From $(\theta_{\text{inc}}, \phi_{\text{inc}})$ to R_{PP}

- From to $(\theta_{\text{inc}}, \phi_{\text{inc}})$ to V_{inc} (incident wave speed)
- From V_{inc} to s_1, s_2 (horizontal slowness)
- From s_1, s_2 to s_3 (vertical slowness)
- From $\underline{s} = (s_1, s_2, s_3)$ to \underline{P} (polarization vector)
- From $\underline{s}, \underline{P}$ to R_{PP} (reflection coefficient)

Schoenberg &
Protázio (1992)

Christoffel equations

$$\Gamma_{ik} = \sum_{jl} c_{ijkl} s_j s_l$$

general Christoffel matrix

Orthorhombic
case

$$\Gamma_{11} = c_{11}s_1^2 + c_{66}s_2^2 + c_{55}s_3^2$$

$$\Gamma_{22} = c_{66}s_1^2 + c_{22}s_2^2 + c_{44}s_3^2$$

$$\Gamma_{33} = c_{55}s_1^2 + c_{44}s_2^2 + c_{33}s_3^2$$

$$\Gamma_{12} = \Gamma_{21} = (c_{12} + c_{66})s_1 s_2$$

$$\Gamma_{13} = \Gamma_{31} = (c_{13} + c_{55})s_1 s_3$$

$$\Gamma_{23} = \Gamma_{32} = (c_{23} + c_{44})s_2 s_3$$

3 X 3 X 3 X 3
 \rightarrow 6 X 6

Christoffel equation

$$(\underline{\Gamma} - \rho \underline{I}) \underline{P} = \underline{0}$$

From to $(\theta_{\text{inc}}, \phi_{\text{inc}})$ to V_{inc}

$$\left(\underline{\underline{\Gamma}} - \rho \underline{\underline{I}} \right) \underline{\underline{P}} = \underline{\underline{0}} \quad \xrightarrow{\times V^2 / \rho} \quad \left(\underline{\underline{\Lambda}} - V^2 \underline{\underline{I}} \right) \underline{\underline{P}} = \underline{\underline{0}}$$

$$\Lambda_{ik} = \sum_{jl} \frac{c_{ijkl}}{\rho} (Vs_j)(Vs_l) = \sum_{jl} a_{ijkl} n_j n_l$$

$$\underline{n} = (\cos \phi_{\text{inc}} \sin \theta_{\text{inc}}, \sin \phi_{\text{inc}} \sin \theta_{\text{inc}}, \cos \theta_{\text{inc}})$$

$$\left| \underline{\underline{\Lambda}} - V^2 \underline{\underline{I}} \right| = 0 \quad \leftarrow$$



In forward modeling, everything is known in this except for V

$$AV^6 + BV^4 + CV^2 + D = 0$$

$$\longrightarrow \quad V_{qP}, V_{qSV}, V_{qSH}$$

(Everything in this slide pertains to the upper layer)

From V_{inc} to s_1, s_2

For an incident P-wave:

$$V_{\text{inc}} = V_{qP}$$

$$\underline{s}_{\text{inc}} = \left\{ \frac{n_1}{V_{qP}}, \frac{n_2}{V_{qP}}, \frac{n_3}{V_{qP}} \right\}$$

By Snell's Law, horizontal slowness components s_1 and s_2 are the same for all reflected and transmitted waves as for the incident wave.

From s_1, s_2 to s_3

$$\Gamma_{11} = c_{11}s_1^2 + c_{66}s_2^2 + c_{55}s_3^2$$

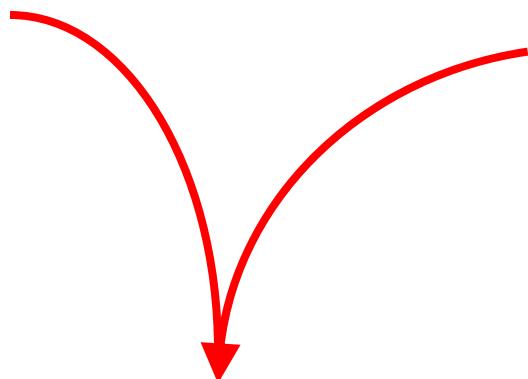
$$\Gamma_{22} = c_{66}s_1^2 + c_{22}s_2^2 + c_{44}s_3^2$$

$$\Gamma_{33} = c_{55}s_1^2 + c_{44}s_2^2 + c_{33}s_3^2$$

$$\Gamma_{12} = \Gamma_{21} = (c_{12} + c_{66})s_1s_2$$

$$\Gamma_{13} = \Gamma_{31} = (c_{13} + c_{55})s_1s_3$$

$$\Gamma_{23} = \Gamma_{32} = (c_{23} + c_{44})s_2s_3$$



$$(\underline{\underline{\Gamma}} - \rho \underline{\underline{I}}) \underline{\underline{P}} = \underline{\underline{0}}$$

$$\left| \underline{\underline{\Gamma}}^U - \rho^U \underline{\underline{I}} \right| = 0 \quad \leftarrow \text{Everything known except } s_3 \rightarrow \left| \underline{\underline{\Gamma}}^L - \rho^L \underline{\underline{I}} \right| = 0$$

$$A^U s_3^6 + B^U s_3^4 + C^U s_3^2 + D^U = 0$$

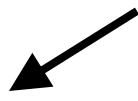
$$A^L s_3^6 + B^L s_3^4 + C^L s_3^2 + D^L = 0$$

$$s_3^{U,qP}, s_3^{U,qSV}, s_3^{U,qSH}$$

$$s_3^{L,qP}, s_3^{L,qSV}, s_3^{L,qSH}$$

From $\underline{s} = (s_1, s_2, s_3)$ to \underline{P}

Everything known except \underline{P}



$$\left(\underline{\underline{\Gamma}}^U - \rho^U \underline{\underline{I}} \right) \underline{P} = \underline{0}$$

$$\left(\underline{\underline{\Gamma}}^L - \rho^L \underline{\underline{I}} \right) \underline{P} = \underline{0}$$

- Only the direction of \underline{P} can be determined uniquely
- The magnitude is arbitrary – determined by normalization
- But use $1 = P_1^2 + P_2^2 + P_3^2$, not $1 = |P_1|^2 + |P_2|^2 + |P_3|^2$

From \underline{s} , \underline{P} to R_{PP}

Schoenberg and Protázio (1992) define two 3 X 3 matrices for each layer:

$$\mathbf{X}^U = \mathbf{X}^U \left(\underline{\underline{c}}^U, \underline{\underline{s}}^U, \underline{\underline{P}}^U \right) \quad \mathbf{X}^L = \mathbf{X}^L \left(\underline{\underline{c}}^L, \underline{\underline{s}}^L, \underline{\underline{P}}^L \right)$$

$$\mathbf{Y}^U = \mathbf{Y}^U \left(\underline{\underline{c}}^U, \underline{\underline{s}}^U, \underline{\underline{P}}^U \right) \quad \mathbf{Y}^L = \mathbf{Y}^L \left(\underline{\underline{c}}^L, \underline{\underline{s}}^L, \underline{\underline{P}}^L \right)$$

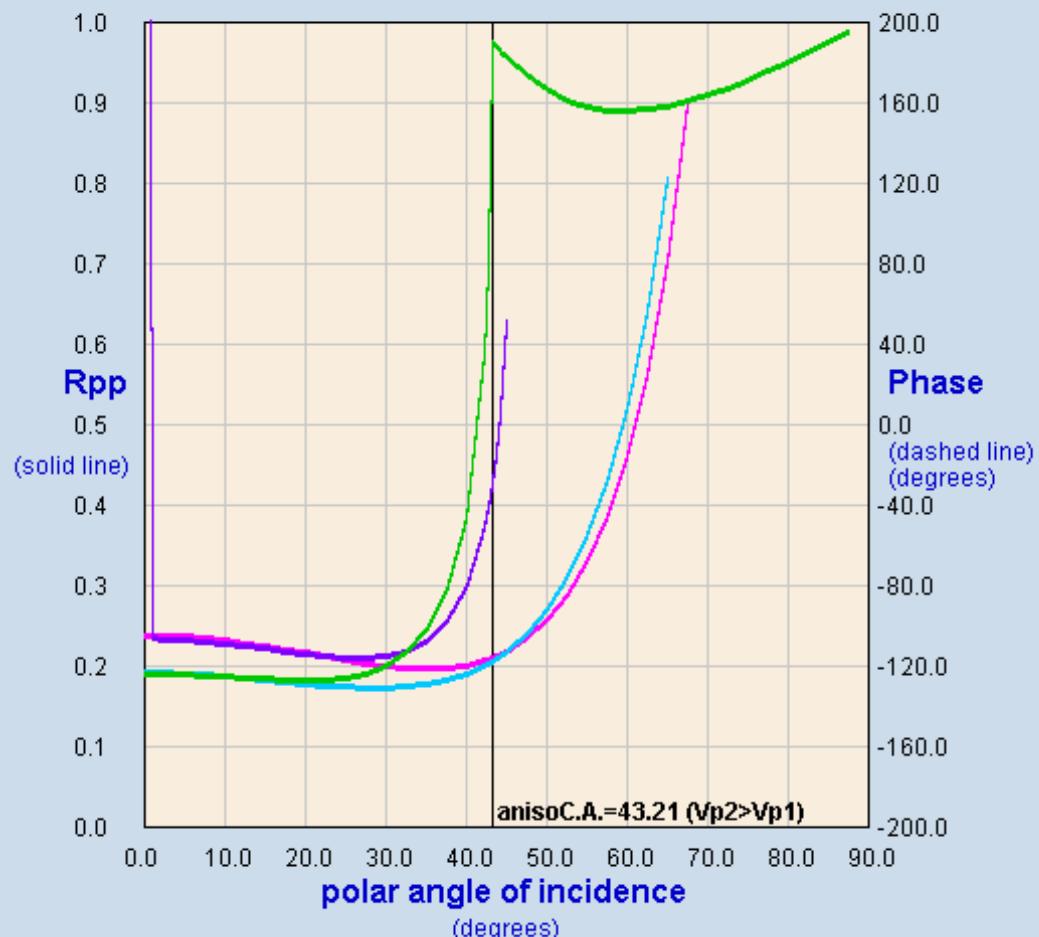
Boundary conditions are encoded in the following expressions:

$$\mathbf{D} = \left(\mathbf{X}^U \right)^{-1} \mathbf{X}^L + \left(\mathbf{Y}^U \right)^{-1} \mathbf{Y}^L$$

$$\mathbf{R} = \begin{bmatrix} R_{PP} & R_{SP} & R_{TP} \\ R_{PS} & R_{SS} & R_{TS} \\ R_{PT} & R_{ST} & R_{TT} \end{bmatrix} = \left[\left(\mathbf{X}^U \right)^{-1} \mathbf{X}^L - \left(\mathbf{Y}^U \right)^{-1} \mathbf{Y}^L \right] \mathbf{D}^{-1} \quad \mathbf{T} = \begin{bmatrix} T_{PP} & T_{SP} & T_{TP} \\ T_{PS} & T_{SS} & T_{TS} \\ T_{PT} & T_{ST} & T_{TT} \end{bmatrix} = 2\mathbf{D}^{-1}$$

CREWES TI Explorer 1.0

www.crewes.org



Upper layer $V_p (\alpha_1)$: 3000.0 m/s

Upper layer $V_s (\beta_1)$: 1500.0 m/s

Lower layer properties:

Lower layer density (ρ_2): 2200.0 kg/m³

Lower layer $V_p (\alpha_2)$: 4000.0 m/s

Lower layer $V_s (\beta_2)$: 2000.0 m/s

Exact Isotropic Aki-Richards

Exact VTI Rüger VTI

Exact HTI Linear HTI

Angle limits (integers, 0 to 90):
0 90

Magnitude limits:
0 1.0

Phase limits (integers):
-200 200

Display magnitude Display phase

Anisotropy Parameters

Azimuth = 45 degrees

Upper layer $\gamma (\gamma_1)$: 0.0

Lower layer $\gamma (\gamma_2)$: 0.1

Upper layer $\delta (\delta_1)$: 0.0

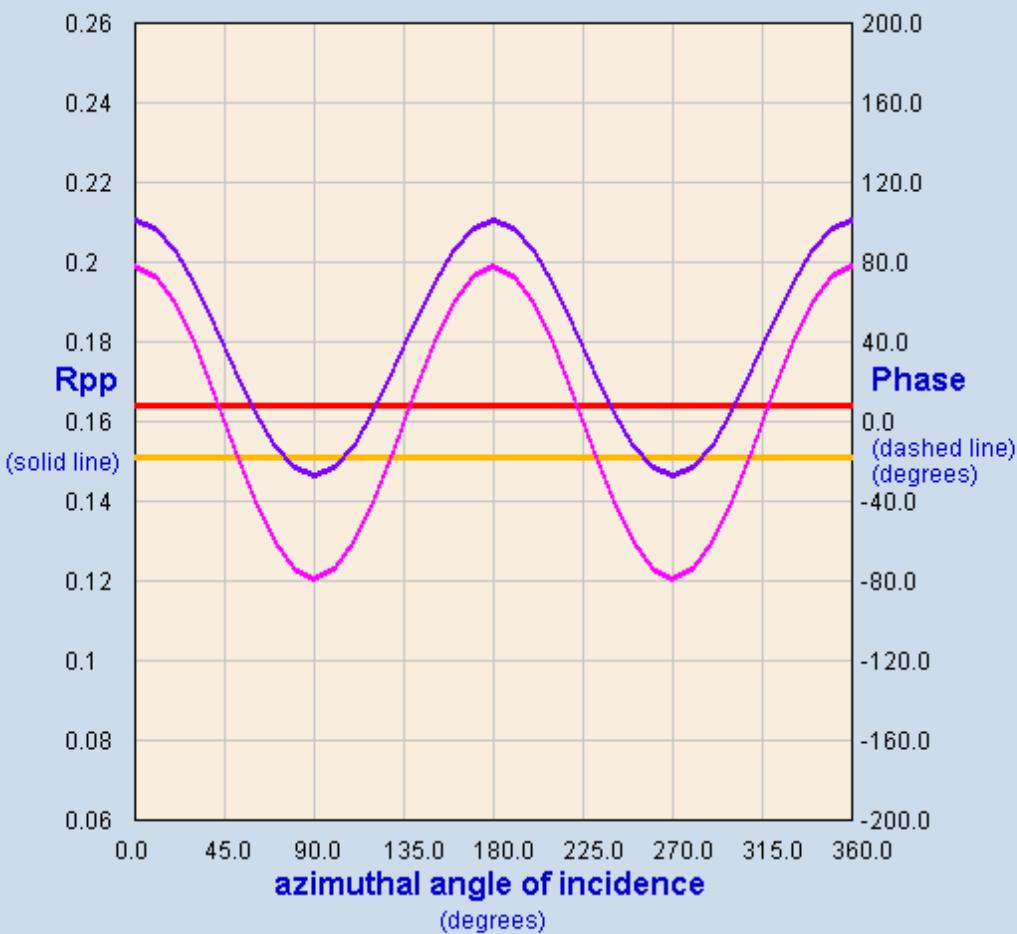
Lower layer $\delta (\delta_2)$: 0.1

Upper layer $\epsilon (\epsilon_1)$: 0.0

Lower layer $\epsilon (\epsilon_2)$: 0.1

CREWES HTI Explorer 1.0

www.crewes.org



Upper layer properties:

Upper layer density (ρ_1): 2000.0 kg/m³

Upper layer V_p (α_1): 3000.0 m/s

Upper layer V_s (β_1): 1500.0 m/s

Lower layer properties:

Lower layer density (ρ_2): 2200.0 kg/m³

Lower layer V_p (α_2): 4000.0 m/s

Lower layer V_s (β_2): 2000.0 m/s

Exact Isotropic

Aki-Richards

Exact HTI

Rüger HTI

Angle limits (integers, 0 to 360): 0 360

Magnitude limits: .06 .26

Phase limits (integers): -200 200

Display magnitude

[Display phase]

Anisotropy Parameters

Polar = 30 degrees

Upper layer γ (γ_1): 0.0

Lower layer γ (γ_2): 0.3

Upper layer δ (δ_1): 0.0

Lower layer δ (δ_2): 0.1

Upper layer ϵ (ϵ_1): 0.0

Lower layer ϵ (ϵ_2): 0.1

Click here to recalculate graph

Units:

m/s, kg/m³ ft/s, g/cm³

Future work

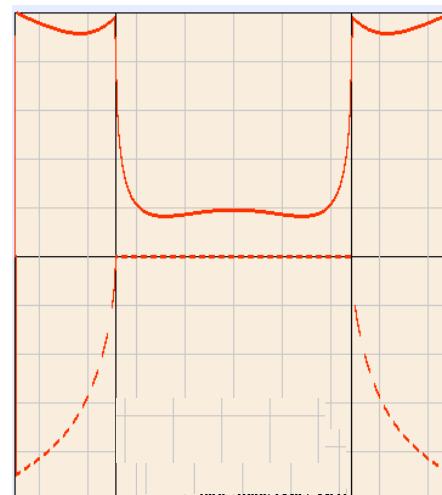
- General improvements (critical angles, post-critical curves, fix instabilities)
- Mixed symmetries (e.g. VTI over HTI)
- Non-aligned HTI media
- Orthorhombic symmetry Explorer
- Studies of linearization
- Reflectivity of point-source waves

Zoepritz Explorer – update

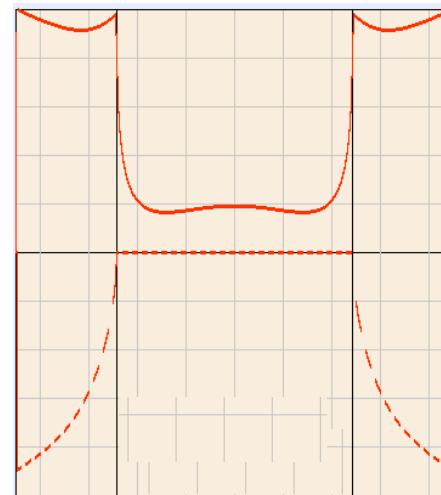
real / imaginary



magnitude / phase

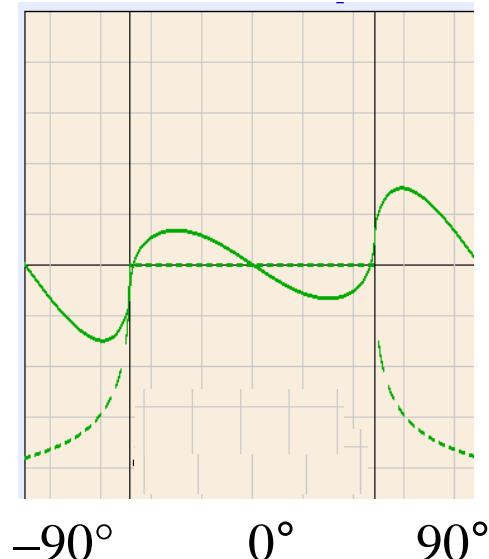
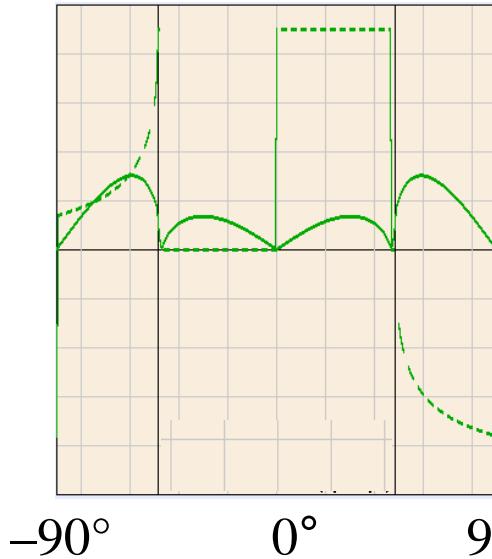
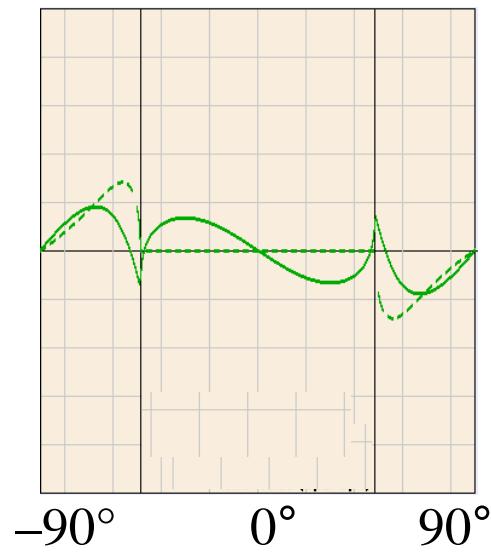


\pm mag. / cts.phase



R_{PP}

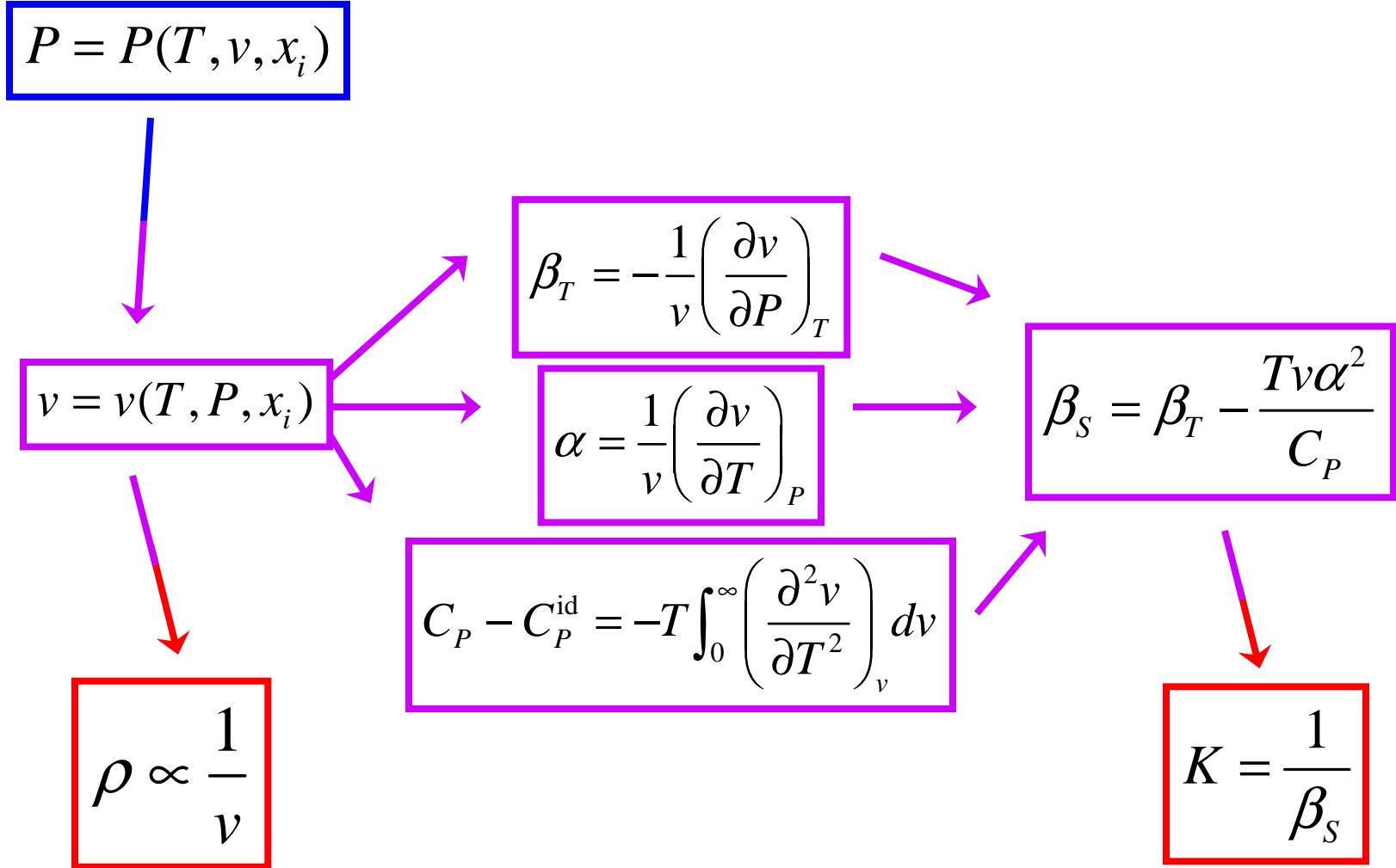
R_{PS}



Acid-gas injection

- Scenario: injection of H_2S and CO_2 in deep saline reservoirs
- Can seismic track progress?
- For fluid substitution, require acoustic properties of acid gas (ρ , V_P)
- Peng-Robinson EOS – non-aqueous

EOS → Acoustic Properties



CREWES Fluid Properties Calculator

1) Enter temperature and pressure of the fluids, and indicate the units

Temperature 40 celsius Kelvin Fahrenheit
Pressure 9.465 MPa bar atm psi kbar

2) Complete calculations individually for each desired fluid (gas, oil and/or brine)

Gas Phase

1. Enter composition:

<input checked="" type="radio"/> by mole fractions: (Solves Peng-Robinson equation of state)	STP density:	<input type="text"/>
CH4 .062	CO2 .745	<input type="radio"/> API <input checked="" type="radio"/> g/cm ³
C2H6 0	H2S .193	<input type="radio"/> L/L <input type="radio"/> % of max
C3H8 0	N2 0	G for saturating gas 0.6
C4H10 0	O2 0	
<input type="radio"/> by density ratio: (B&W, 1992) G .6		

2. [Click here to calculate gas properties](#)

3. Calculated gas properties

Density: 0.43216807 g/cm³

432.16806 kg/m³ 26.979376 lb/ft³

Acoustic speed: 277.0641 m/s

0.27706409 km/s 909.0029 ft/s

Bulk modulus: 33.17517 MPa

0.33175173 kbar 4811.654 psi

Viscosity: 0.0 cP

0.0 Poise

3) Complete calculations for multiphase mixtures (single-phase calculations above must be completed first):

1. Enter volume fractions for each phase:

Gas

Oil

Brine

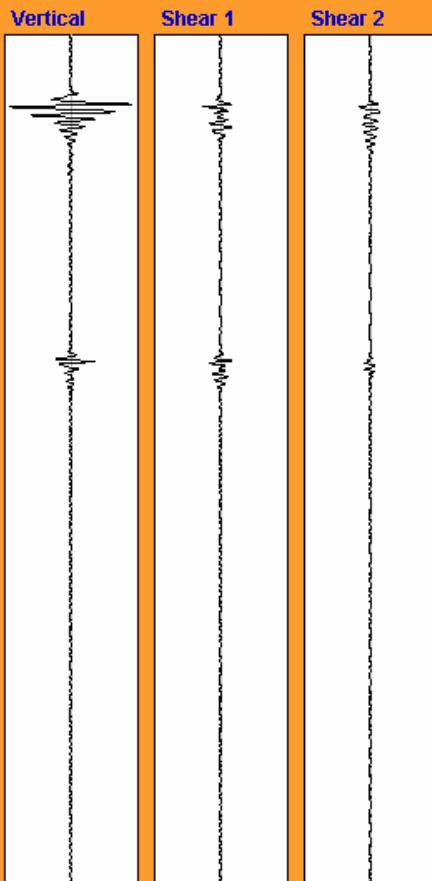
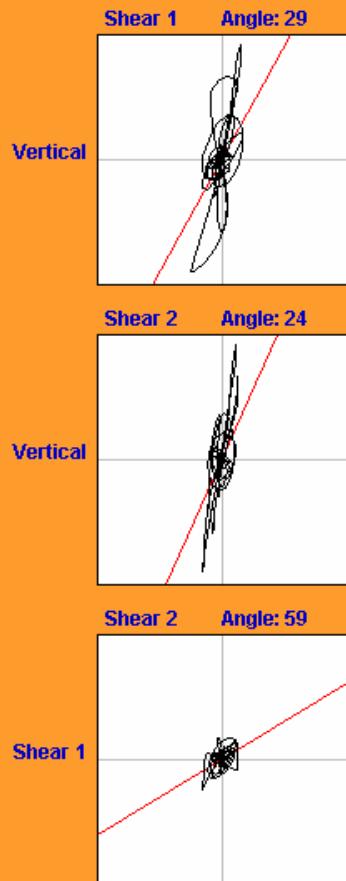
2. [Click here to calculate multiphase properties](#)

3. Calculated mixture properties

Density:

Acoustic speed:

CREWES Hodogram Explorer 1.0



0.0 2048.0

1) Copy and paste columns of ASCII data in box below:

On a PC, type Ctrl-A and Ctrl-C in the ASCII file, then Ctrl-A and Ctrl-V in the box below					
219236	1	7252	2041.00	2042	-2.79647111e-007
219237	1	7252	2042.00	2043	-5.41181805e-007
219238	1	7252	2043.00	2044	-7.07775826e-007
219239	1	7252	2044.00	2045	-7.20713274e-007
219240	1	7252	2045.00	2046	-5.28443422e-007
219241	1	7252	2046.00	2047	-2.18343644e-007
219242	1	7252	2047.00	2048	2.56757815e-008
219243	1	7252	2048.00	2049	1.0947042e-007

2) Check off columns to be read, and change col.# as required:

Data:

Col #:

 6

3) Click button to read data:

Number of elements read: t: 2049, P: 2049, S1: 2049, S2: 2049

4) Repeat 1)-3) until four columns have been read

5) Click button to plot hodograms:

Options: color scheme (below); plot limits (at left)

Black on White

CREWES Hodogram Explorer 1.0

